

## **CONTENT THIS CHAPTER**

**\*ENERGY COMPLIANCE**\_REQUIRED COMPLIANCES ARE BEST UNDERSTOOD UPFRONT ON ANY PROJECT. ENERGY COMPLIANCE HAS SEVERAL OPTIONS WHICH ARE OVERVIEWED THIS CHAPTER. SOME REQUIRE 3RD PARTY INVOLVEMENT.

**\*LIMITED TO THE CONCEPT OF MANAGING HEAT GAIN AND HEAT LOSS**\_INSTRUCTIVE CONCEPTS ARE NOTED THIS CHAPTER ABOUT HEAT GAIN/HEAT LOSS INTENDED TO ESTABLISH AN OVERVIEW LOGIC ABOUT HOW TO CONDITION A HOME INTELLIGENTLY AND EFFICIENTLY. THIS, IN TURN MAY HELP IN BETTER/BEST SYSTEM AND ENERGY SOURCE SELECTION FOR A GIVEN LOCATION, HOME SIZE, AND GEOMETRY.

**\*DUCTED SYSTEMS**\_THE DESIGNS THIS PROJECT DEFAULT TO DUCTED AIR SYSTEMS (d8.15, d8.16). SPACE FOR AIR HANDLERS AND SOMETIMES DUCTING. DUCTING IS ADMITTEDLY DIFFICULT TO DESIGN FOR WITHOUT HAVING OTHER PROJECT SPECIFIC CRITERIA, MOST NOABLY THE BOUNDARIES OF THE THERMAL ENVELOPE. THIS DEFAULT SITUATION EXPLAINS THE EFFORT THIS CHAPTER TO OUTLINE DUCTWORK OPTIONS. DUCTED SYSTEMS ALLOW A RANGE OF SYSTEM SELECTIONS. FUEL FIRED FURNACES, , HEAT PUMP HEATING AND COOLING, AND AC SYSTEMS INDEPENDENT OF HYDRONIC HEATING SYSTEMS, ALL REQUIRE DUCTING. HAVING NOTED THE FORCED AIR SYSTEM DEFAULT THINKING, THERE IS NOTHING PREVENTING THESE PROJECTS DESIGNS FROM BEING HEATED AND OR COOLED SOME OTHER PERFECTLY VALID WAY.

**\*NOT ATTEMPTED THIS CHAPTER OR PROJECT**\_ARE ALTERNATIVE SYSTEM SUMMARIES, OR ENERGY SOURCE OPTIONS, INDOOR AIR QUALITY, OR MAKE UP AIR SYSTEMS. THE SUBJECT IS SIMPLY TOO VAST AND COMPLICATED AND FAR BETTER LEFT TO OTHER APPROPRIATE RESOURCES. THE CHAPTER DOES INTRODUCE AN EXPANSIVE COTTAGE INDUSTRY OF ENERGY, BUILDING SCIENCE, GREEN CONSTRUCTION CONSULTANTS WHOM ARE BECOMING CRITICAL TO THE HOME BUILDING INDUSTRY.

## **RELATED CONTENT WITHIN THE GUIDE(S)**

**\*d2.3-d2.7**\_mother nature's rules

**\*d4.5-d4.6**\_designing with the sun in mind

**\*d5.1**\_thermal envelope and house geometrey

**\*d5.3-d5.5**\_space under roof

**\*d8.15-d8.16**\_mep space allocations

**\*c3.13-c3.14**\_foundation and slab heat gain and loss

**\*c5.23-c5.24**\_frame floor insulation assemblies

**\*c6.16-c6.21**\_frame wall insulation assemblies

**\*c7.25-c7.27**\_frame roof insulation assemblies

**\*the addendum drawing set shows conventional 2d section options**

## **c9.1 DEFINING THE THERMAL ENVELOPE**

## **c9.2 SURFACE AREA, DELTA T, AND R**

## **c9.3 LEARNING FROM THE LOAD FORMULA**

## **c9.4 R values, U values AND CODE COMPLIANCE**

## **c9.5 UA COMPLIANCE AND REScheck1**

## **c9.6 UA COMPLIANCE AND REScheck2**

## **c9.7 AIR TIGHTNESS AND THE STACK EFFECT**

## **c9.8 AIR TIGHTNESS AND CODE COMPLIANCE**

## **c9.9 DUCTING REQUIREMENTS**

## **c9.10 CONDITIONED SPACE DUCTING OPTIONS**

## **c9.11 CEILING PLANE DUCTING OPTIONS**

## **c9.12 HVAC RULES OF THUMB**

## **c9.13 CODE COMPLIANCE AND GLASS**

## **c9.14 SOLAR HEAT GAIN AND GLASS**

## **c9.15 CODE COMPLIANCE OVERVIEW**

## **c9.16 SUMMARY THOUGHTS**

# THERMAL ENVELOPE c9.1

## DEFINING THE THERMAL ENVELOPE

### QUALIFY

**\*CRITERION** THESE ILLUSTRATIONS SHOW THE SAME PHYSICAL SHELL FOR 3 COMMON CONFIGURATIONS, WITH 2 OPTIONS FOR DEFINING THE THERMAL ENVELOPE. THE 2 LEADING CRITERIA FOR SELECTING THE THERMAL ENVELOPE APPROACH IS WHETHER USEFUL SPACE IS GAINED, AND WHAT IS REQUIRED TO INCORPORATE THE HVAC SYSTEM WITHIN THAT THERMAL ENVELOPE. (THIS CHAPTER WILL EMPHASIZE THE IMPORTANCE OF THAT INCLUSION.)

**\*INVESTMENT** FINISHING AND OR CONDITIONING MORE SPACE WITHIN THE SAME PHYSICAL ENVELOPE OBVIOUSLY COSTS MORE MONEY UP FRONT. ENERGY COSTS WILL BE LOWER WITH AN INCORPORATED SYSTEM. A COST BENEFIT ANALYSIS IS SMART.

### QUANTIFY

**\*SURFACE SQUARE FOOTAGE** MATTERS A LOT. EVERY SQUARE FOOT THAT SEPARATES THE CONDITIONED INSIDE FROM UNCONDITIONED OUTSIDE IS A SQUARE FOOT SUBJECT TO HEAT LOSS AND HEAT GAIN.

**\*VOLUME** SYSTEM EFFICIENCY AND DESIGN DOES NOT CARE DIRECTLY ABOUT SPACE VOLUME (CU FT). BUT IT CLEARLY HAS A DIRECT RELATIONSHIP TO SURFACE AREA. MORE VOLUME=MORE SURFACE AREA. NO WAY AROUND IT.

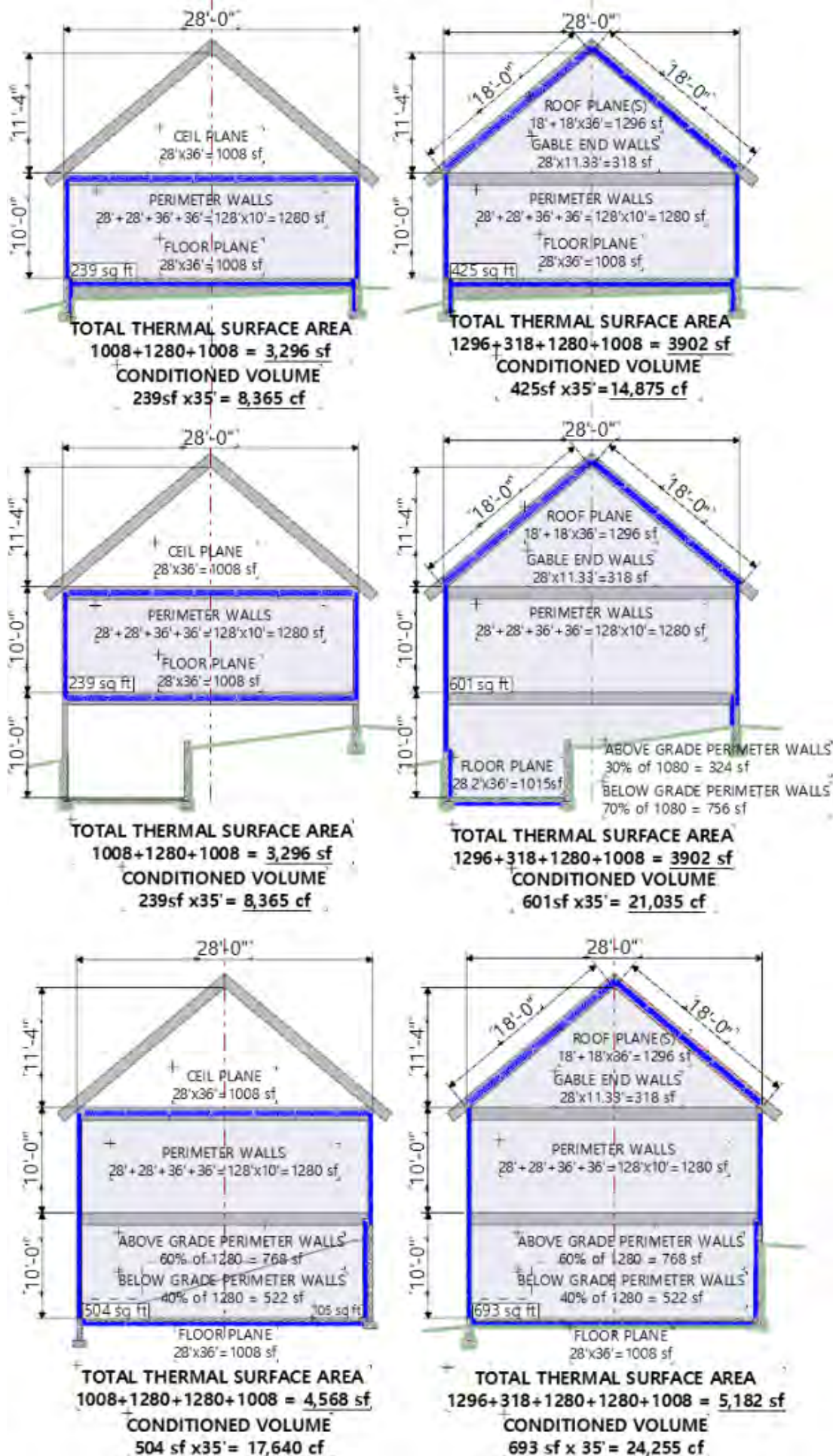
**\*DELTA T (c9.2)** EACH SQUARE FOOT OF SURFACE CONSTRUCTION IS SEPARATING 2 TEMPERATURES. THERE IS AN INSIDE (DESIRED) TEMPERATURE AND AN OUTSIDE TEMPERATURE THAT HAS A MIND OF ITS OWN. THE DIFFERENCE BETWEEN THOSE 2 TEMPERATURES IS TYPICALLY REFERRED TO AS DELTA (DIFFERENT) T (TEMPERATURE).

**\*RESISTANCE** LOGIC SAYS WE CAN SLOW DOWN THE HEAT GAIN AND LOSS BY CONSTRUCTING ALL THAT SURFACE AREA WITH ADEQUATE INSULATION WHICH IS THE RESISTANCE COMPONENT.

**\*LOAD** IS THE DEMAND ASKED OF A HEATING AND COOLING SYSTEM TO MAINTAIN THAT DESIRED INSIDE TEMPERATURE. THE LOAD IS QUANTIFIED AND IS A DIRECT FUNCTION OF SURFACE AREA(S) AND ITS RESISTANCE(S), WHILE DEALING WITH THAT DELTA T CHALLENGE.

### THE LOAD FORMULA

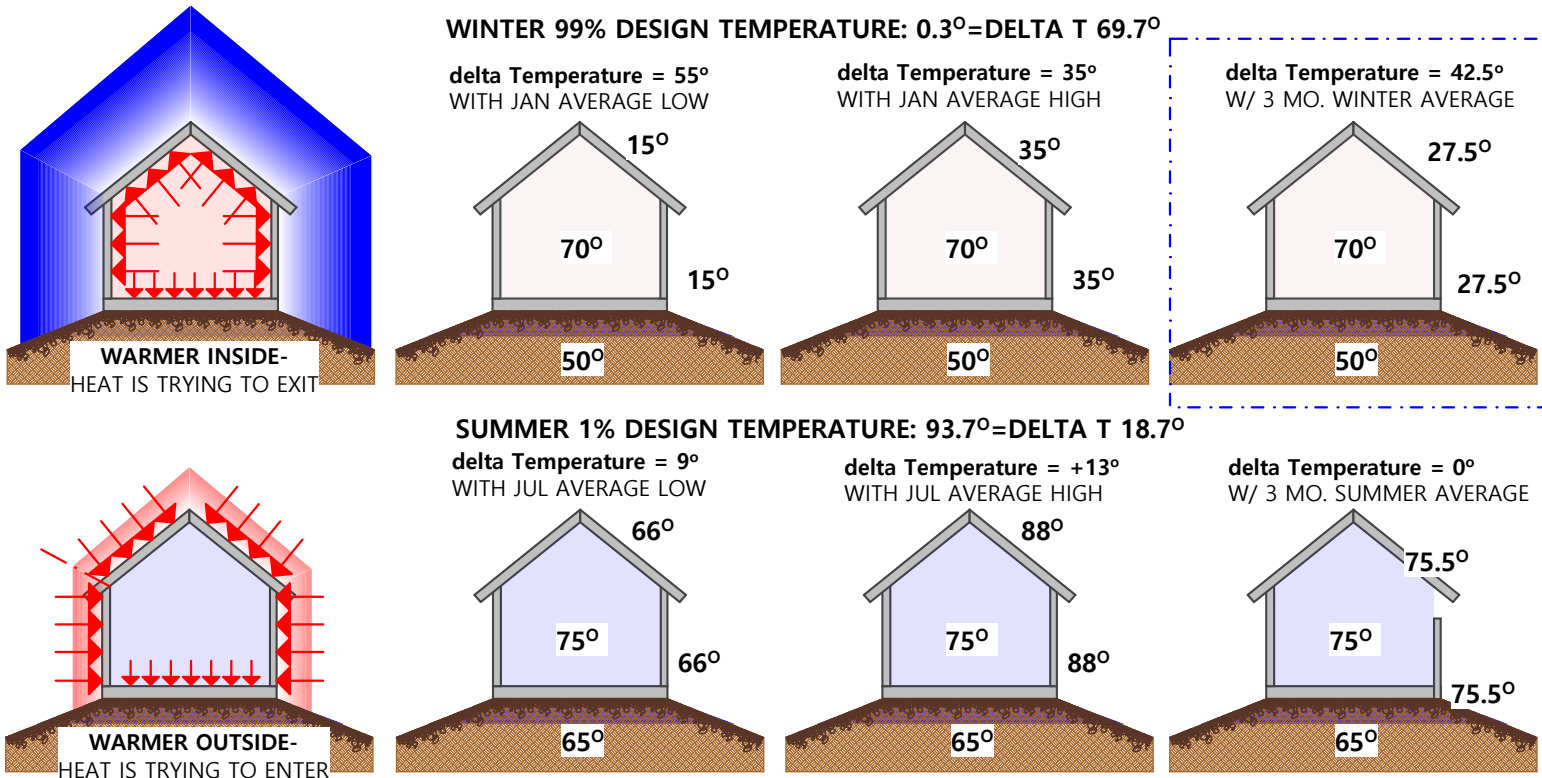
**\*LOAD FORMULA IS SURFACE AREA TIMES THE DELTA T DIVIDED BY THE UNIT RESISTANCE VALUE OF EACH SQUARE FOOT** THIS SIMPLE FORMULA IS A GREAT ONE TO REMAIN MINDFUL OF WHILE MAKING THERMAL ENVELOPE DECISIONS. AS WITH SO MUCH OF THIS STUFF THERE ARE LAYERS OF COMPLICATION, BUT THIS CORE FORMULA IS A KIND OF GUIDE POST.



### BASIC LOAD EQUATION IS SURFACE AREA X DELTA T / R VALUE

\*FIND OUT WHERE THE ENERGY IS GOING, RECOGNIZING THE 3 VARIABLES, THE SQUARE FOOT, THE INSULATING VALUE OF THAT SQUARE FOOT, AND TEMPERATURE DIFFERENTIAL THAT SQUARE FOOT IS ADDRESSING, ALLOWS ONE TO WALK THRU A HOME AND CONSIDER WHERE THE HEAT IS ESCAPING (HEAT LOSS), AND, DURING HOTTER SUMMER MONTHS, WHERE THE HEAT IS ENTERING (HEAT GAIN).

\*DELTA T, THE DIFFERENCE BETWEEN THE INSIDE DESIRED TEMPERATURE AND THE OUTSIDE REAL TEMPERATURE CREATES THE DEMAND. MORE TEMPERATURE DIFFERENTIAL MORE DEMAND. LIVING IN SAN DIEGO AND HAWAII HAS CLEAR ADVANTAGES IN THIS REGARD. LIVING IN MINNESOTA OR SOUTH TEXAS DOES NOT.



### TEMPERATURES REFERENCES ABOVE

\*LINCOLN NEBRASKA, A TYPICAL WEATHER CONDITION, MIDDLE OF THE COUNTRY, AND IN CODE DEFINED ZONE 5a. ABOVE NOTES SOME DELTA TEMPERATURES IN LINCOLN. EVERYDAY TEMPERATURES ARE EASILY SEARCHED. (SEARCH 'AVERAGE TEMPERATURES BY MONTH'-THAT SIMPLE)

\*DESIGN TEMPERATURES, TAKE THE RECORDED EVERYDAY TEMPERATURE DATA AND ESTABLISH AN ALMOST EXTREME WINTER AND SUMMER TEMPERATURE NUMBER THAT IS USED TO ESTABLISH HEATING AND COOLING LOADS. WHICH IN TURN DIRECTS HVAC SYSTEM DESIGNS.

\*OBSERVATION, USING REAL TEMPERATURES THE 3 MONTH (DEC/JAN/FEB) WINTER AVERAGE IS 27.5° AND THE 3 MONTH (JUN/JUL/AUG) SUMMER MONTH AVERAGE IS 75.5°. SO (DUH) LINCOLN CALLS FOR HEAT A LOT MORE THAN COOLING. KNOWING THAT SIMPLE DISTINCTION BETWEEN A HEAT LOSS DOMINANT CLIMATE LOCATION, OR A HEAT GAIN DOMINANT CLIMATE LOCATION IS USUALLY OBVIOUS BUT STILL IMPORTANT TO KEEP FRONT AND CENTER WHEN MAKING HVAC SYSTEM DECISIONS. IT IS A DIFFERENT CRITERIA SET.

\*OBSERVATION, THE DESIGN TEMPERATURES ARE CLEARLY HIGHER AND LOWER THAN THE AVERAGES. BUT THEY NEED TO ADDRESS WORST CASE SCENARIOS-WHICH OF COURSE REPRESENT THE TEMPERATURES OF GREATEST POTENTIAL DISCOMFORT AND EVEN HEALTH AND SAFETY RISKS. THERE IS A CHALLENGE WITH SETTING DESIGN TEMPERATURES (THEREFORE EQUIPMENT SIZING). OVERSIZED EQUIPMENT RUNS INEFFICIENTLY. NOT BEING ABLE TO ACHIEVE ADEQUATE HEATING OR COOLING IN EXTREME CONDITIONS IS A PROBLEM. THERE ARE 3 SLIGHTLY DIFFERENT DESIGN TEMPERATURES THE HVAC GURUS LIST IN THEIR TABLES, WITH THE 'MIDDLE' 99%/1% SEEMING TO BE THE DEFAULT.

### RUNNING THE load FORMULA

#### \*SQUARE FOOTAGE

ROOF AREA\_1296 SF  
WALLS\_1800 SF  
FLOOR AREA\_1008 SF

#### \*RESISTANCE R

ROOF AREA\_R 49 (TO KEEP THINGS SIMPLE LETS SAY THERE IS ONE ROOF CONSTRUCTION/1 UNIFORM R VALUE AND NO SKYLIGHTS)  
WALLS\_R-20 (TO KEEP THINGS SIMPLE LETS SAY THERE ARE NO DOORS OR WINDOWS)  
FLOOR\_R-10 (TO KEEP THINGS SIMPLE LETS SAY THIS TOTAL SLAB AREA IS INSULATED)

#### \*DELTA T FOR THE 3 MONTH WINTER AVERAGE 27.5°

roof area (1296) x delta T (42.5) / R value (49) = heat flow (1124 BTU/hr)  
wall area (1598) x delta T (42.5) / R value (20) = heat flow (3396 BTU/hr)  
floor area (1008) x delta T (20) / R value (10) = heat flow (2016 BTU/hr)  
total btu's per hr to maintain temperature equilibrium in the winter months = **6536 BTU/hr**

#### \*THE LOAD (BTU/hr)

THE 'LOAD' IS ONE OF THE TERMS USED TO DESCRIBE THE ENERGY REQUIREMENT NEEDED TO BALANCE THE 2 TEMPERATURES. THE LOAD CALCULATED HERE REPRESENTS THE REQUIREMENT FOR A 42.5° DELTA T. THE ACTUAL LOAD ON AN HOUR TO HOUR, DAY TO DAY, BASIS IS ALWAYS CHANGING WITH THE SIMPLE CHANGE OF TEMPERATURE. THE BTU/hr (BRITISH THERMAL UNIT) IS A FIXED ENERGY MEASUREMENT. SEARCH ITS DEFINITION AND HISTORY FOR INTEREST SAKE BUT ALSO NOTE IT IS ULTIMATELY A NUMERICAL TOOL FOR CIPHERING OTHER END DECISIONS.

### PLAYING WITH THE load FORMULA

**\*BELOW FORMULA RUNS** ARE ONLY EMPHASIZING THAT GETTING A HANDLE ON HEAT GAIN AND LOSS IS NOT ROCKET SCIENCE. REMEMBER RUNNING REAL SEASONAL TEMPERATURE AVERAGES WILL INFORM ABOUT SEASONAL ENERGY CONSUMPTION, RUNNING 'DESIGN TEMPERATURES' WILL INFORM ABOUT SYSTEM CAPACITY REQUIREMENTS. RUNNING SQUARE FOOTAGE AND R VALUE VARIABLES WILL INFORM ABOUT DESIGN DECISIONS VERY MUCH IN ONE'S CONTROL.

**\*CAVEAT** THESE EXERCISES ILLUSTRATE THE BASE FORMULA AT WORK ONLY. REAL CONDITIONS AND CONSIDERATIONS ARE MORE COMPLEX, BUT STILL SIMPLER THAN ROCKET SCIENCE. THE REScheck TOOL (c9.5,c9.6) ALLOWS MORE ACCURATE "PLAYING" AND IS LAYMAN SIMPLE. THE REScheck TOOL CONSIDERS/INCORPORATES VARYING CONSTRUCTIONS AND R VALUES IN THE ROOF, WALL, AND FLOOR ASSEMBLIES.

**\*SAME SQUARE FOOTAGES\_**

**\*SAME RESISTANCE R\_**

**\*DIFFERENT DELTA T FOR THE AVERAGE HIGH IN AUGUST OF 88°=13°**

roof area (1296) x delta T (13) / R value (38) = heat flow (443 BTU/hr)

wall area (1598) x delta T (13) / R value (20) = heat flow (1038 BTU/hr)

floor area (1008) x delta T (10) / R value (10) = heat flow (1008 BTU/hr)

total btu's per hr to maintain temperature equilibrium in high august temperatures = **2489 BTU/hr**

**\*\*\*OBSERVATION**\_DELTA T CONTROLS ENERGY CONSUMPTION. WE ALL KNOW JANUARY AND AUGUST ARE CONSUMING MONTHS. MAY AND OCTOBER NOT SO MUCH.

**\*SAME SQUARE FOOTAGES\_**

**\*SAME RESISTANCE R\_**

**\*DIFFERENT DELTA T FOR THE SUMMER DESIGN TEMPERATURE 93.7°=18.7°**

roof area (1296) x delta T (18.7) / R value (38) = heat flow (638 BTU/hr)

wall area (1598) x delta T (18.7) / R value (20) = heat flow (1494 BTU/hr)

floor area (1008) x delta T (10) / R value (10) = heat flow (1008 BTU/hr)

total btu's per hr to maintain temperature equilibrium summer design temperature = **3140 BTU/hr**

**\*\*\*OBSERVATION**\_THE CODE REQUIRED USE OF THE SUMMER DESIGN TEMPERATURE PROVIDES A 25%+/- BUFFER OVER THE HIGH AVERAGE IN AUGUST.

**\*SAME SQUARE FOOTAGES\_**

**\*SAME RESISTANCE R\_**

**\*DELTA T FOR THE 3 MONTH WINTER AVERAGE 42.5°**

roof area (1296) x delta T (42.5) / R value (49) = heat flow (1124 BTU/hr)

wall area (1598) x delta T (42.5) / R value (20) = heat flow (3396 BTU/hr)

floor area (1008) x delta T (20) / R value (10) = heat flow (2016 BTU/hr)

total btu's per hr to maintain temperature equilibrium in the winter months = **6536 BTU/hr**

**\*\*\*OBSERVATION**\_THIS 3 MONTH AVERAGE LOAD HAS A 33% BUFFER COMPARED WITH THE WINTER DESIGN REQUIREMENT

**\*SAME SQUARE FOOTAGES\_**

**\*INCREASE THE RESISTANCE R\_**

**\*DELTA T FOR THE 3 MONTH WINTER AVERAGE 42.5°**

roof area (1296) x delta T (42.5) / R value (60) = heat flow (918 BTU/hr)

wall area (1598) x delta T (42.5) / R value (25) = heat flow (2716 BTU/hr)

floor area (1008) x delta T (20) / R value (10) = heat flow (2016 BTU/hr)

total btu's per hr to maintain temperature equilibrium in the winter months = **5650 BTU/hr**

**\*\*\*OBSERVATION**\_INCREASING THE ROOF R BY 10 AND THE WALL R BY 5 DECREASES LOAD BY 15%

**\*ALTER SQUARE FOOTAGES\_**

**\*SAME RESISTANCE R\_**

**\*DELTA T FOR THE 3 MONTH WINTER AVERAGE 42.5°**

roof area (1008) x delta T (42.5) / R value (49) = heat flow (874 BTU/hr)

wall area (1598) x delta T (42.5) / R value (20) = heat flow (3396 BTU/hr)

floor area (1008) x delta T (20) / R value (10) = heat flow (2106 BTU/hr)

total btu's per hr to maintain temperature equilibrium in the winter months = **6376 BTU/hr**

**\*\*\*OBSERVATION**\_INSULATING THE CEILING INSTEAD OF THE THE ROOF PLANE REDUCES THE ROOF SURFACE AREA FROM 1296 TO 1008 OR 22%. BECAUSE THIS BECOMES INCORPORATED INTO THE ENTIRE ROOF/WALL/FLOOR SQUARE FOOTAGE PACKAGE THAT PERCENTAGE OF DECREASE BECOMES LESS.

SAME DELTA T THIS EXERCISE

### THE PRINCIPLE -BTU'S, ENERGY SOURCES, AND COSTS

**\*JUMPING AHEAD**\_NOTED THE EXERCISES ABOVE ARE TOO SIMPLE TO CIPHER ACTUAL BTU REQUIREMENTS. BUT THE CONCEPT OF THE BTU BEING THE UNIT OF CONSIDERATION FOR ENERGY SOURCES AND ULTIMATELY ENERGY COSTS IS VALID AND SUMMARIZED BELOW TO EMPHASIZE THAT ACTUAL BTU CONSUMPTION IS THE BOTTOM LINE BOTH REGARDING ENERGY CONSERVATION AND ENERGY COST.

**\*STARTING WITH THE BTU**\_THE HEAT LOSS/HEAT GAIN CALCS CAN RESULT IN AN ANNUAL EDUCATED ESTIMATE SUMMARY DEMAND. ENERGY SOURCES HAVE RECOGNIZED BTU OUTPUT PER UNIT OF CONSUMPTION. UNIT OF CONSUMPTION HAS A MARKET PRICE. ANNUAL ENERGY COSTS CAN BE CONCLUDED.

**\*FUEL OIL**\_134,900 BTU/GAL = 'X' GALLONS ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*PROPANE**\_91,600 BTU/GAL = 'X' GALLONS ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*NATURAL GAS**\_1,000 BTU/CU FT = 'X' CU FT ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*BIOGAS**\_600 BTU/CU FT = 'X' CU FT ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*HARDWOOD**\_24,000,000 BTU/CORD= 'X' CORDS ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*WOOD PELLETS**\_8,200 BTU/LB='X' LBS ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*COAL**\_13,000 BTU/LB = 'X' LBS ANNUALLY X \$UNIT COST = \$ANNUAL COST

**\*ELECTRICITY**\_3,412 BTU/kWH = 'X' kWH ANNUALLY X \$UNIT COST = \$ANNUAL COST

### R (RESISTANCE) AND U (TRANSMITTANCE) ARE THE SAME THING -SORT OF-

**\*RESISTANCE AND TRANSMITTANCE**\_ARE 2 SIDES OF THE SAME COIN. THEY ARE USED A BIT DIFFERENTLY.

**\*MATH**\_THESE 2 VALUES ARE MATHEMATICAL RECIPROCALLS. DIVIDE 1 BY THE R VALUE AND YOU GET THE U VALUE. DIVIDE 1 BY THE R VALUE AND YOU GET THE R VALUE. HIGHER R VALUES MEAN MORE RESISTANCE. HIGHER IS BETTER. HIGHER U VALUES MEAN MORE HEAT IS ESCAPING, SO WITH THE U VALUE LOWER IS BETTER.

**\*R THINKING**\_MOST OF US THINK IN TERMS OF R-THE INSULATING VALUE. EASY. THE BIGGER THE NUMBER THE MORE EFFECTIVE. THE CODE DICTATES A MIN R BY COMPONENT. IT IS REFERRING TO THE INSULATING PRODUCT'S R VALUE ONLY. NOT THE WHOLE CONSTRUCTION ASSEMBLY. ALL MATERIALS HAVE A SEARCHABLE R-VALUE USUALLY/FREQUENTLY QUANTIFIED BY A UNIT OF THICKNESS. INSULATION MATERIALS LOUDLY MARKET THEIR R VALUES. R VALUES TYPICALLY REPRESENT A RESISTANCE VALUE OF 1 HOMOGENEOUS MATERIAL.

**\*U THINKING**\_RECIPROCAL VALUE ASIDE , A U VALUE IS MORE FREQUENTLY USED REPRESENTING A COMPOSITE OR ASSEMBLY. AND TAKES INTO ACCOUNT TRANSMITTANCE CONDITIONS THE R VALUE DOES NOT. FOR EXAMPLE, GLAZING PRODUCTS ARE USUALLY SPECIFIED BY U VALUE. THE U VALUE CONSIDERS THE GLASS, THE FRAME, THE GLASS TO FRAME CONNECTION, (AND OTHER TECHNICAL STUFF), AND CONCLUDES A U VALUE FOR THE ENTIRE ASSEMBLY ON A PSF BASIS. ULTIMATELY THE U VALUE FIGURES INTO THE BTU CALCS THE SAME WAY WITH THE ADVANTAGE OF HAVING ITS BASE VALUE MORE ACCURATE, WHICH IS GOOD. THAT U VALUE CAN BE TRANSLATED INTO AN R VALUE TO HELP PUT THE WINDOW IN PERSPECTIVE WITH THE OTHER ASSEMBLIES. USING THE RECIPROCAL RULE-ZONE 5 U VALUE REQUIRED FOR FENETRATION IS .30. THE EQUIVALENT R VALUE IS 1 DIVIDED BY .30 OR 3.33. SO COMPARE R-3.33 FOR GLAZING WITH THE THE REQUIRED R-20 WALL AND THE R-49 CEILING/ROOF. USING R'S DOES HELP KEEP THINGS IN PERSPECTIVE.

ANOTHER ILLUSTRATION OF THIS R AND U DISTINCTION IS THE FRAME WALL REQUIREMENT. COMPONENT IN ZONE 3 THRU 5 IS R-20 CAVITY INSULATION . BUT THE RECIPROCAL (U VALUE EQUIVALENT) OF 20 IS .050. THE U FACTOR CODE REQUIREMENT FOR THAT SAME FRAME WALL IS .060. THAT RECIPROCAL (R VALUE EQUIVALENT) OF THAT U=0.60 IS R=16.68. WHY THE DISCREPANCY? BECAUSE THE U FACTOR REQUIREMENT IS CONSIDERING THE ASSEMBLY, WHICH INCLUDES THE MORE EFFICIENT INSULATION ITSELF, AND THE LESS EFFICIENT FRAMING COMPONENT. (c6.17) DEMONSTRATES THE EFFICIENCY FACTORS ASSOCIATED WITH FRAME WALLS WHICH EXPLAINS THE R DE-VALUATION FROM 20 TO 16.68.

THERE ARE MORE VARIABLES HERE IF ONE WANTS TO BE REALLY EXACTING. A 3RD PARTY ATTEMPTING HIGHLY ACCURATE ENERGY PERFORMANCE CODE COMPLIANCES MAY WANT TO DIG DEEPER.

**\*U(A) THINKING**\_REScheck PRESENTS US WITH A 'UA' NUMBER REPRESENTING THE ASSEMBLY U VALUE TIMES THE AREA. IT RUNS A BEHIND THE SCENES CALC TO GENERATE THE U VALUE AND MULTIPLIES IT BY THE SQUARE FOOTAGE INPUT.

**\*MEETING CODE**\_A PROJECT THAT MEETS THE R OR U VALUE REQUIREMENTS SHOULD BE ENERGY ACCEPTABLE.

TABLE N1102.1.2 (R402.1.2)  
INSULATION AND FENESTRATION REQUIREMENTS BY COMPONENT\*

CLIMATE ZONE	FENESTRATION U-FACTOR <sup>a</sup>	SKYLIGHT <sup>b</sup> U-FACTOR	GLAZED FENESTRATION SHGC <sup>c,4</sup>	CEILING R-VALUE	WOOD FRAME WALL R-VALUE	MASS WALL R-VALUE <sup>e</sup>	FLOOR R-VALUE	BASEMENT <sup>d</sup> WALL R-VALUE	SLAB <sup>f</sup> R-VALUE & DEPTH	CRAWL SPACE <sup>g</sup> WALL R-VALUE
1	NR	0.75	0.25	30	13	3/4	13	0	0	0
2	0.40	0.65	0.25	38	13	4/6	13	0	0	0
3	0.32	0.55	0.25	38	20 or 13 + 5 <sup>h</sup>	8/13	19	5/13 <sup>i</sup>	0	5/13
4 except Marine	0.32	0.55	0.40	49	20 or 13 + 5 <sup>h</sup>	8/13	19	10/13	10, 2 ft	10/13
5 and Marine 4	0.30	0.55	NR	49	20 or 13 + 5 <sup>h</sup>	13/17	30 <sup>j</sup>	15/19	10, 2 ft	15/19
6	0.30	0.55	NR	49	20 + 5 <sup>h</sup> or 13 + 10 <sup>h</sup>	15/20	30 <sup>j</sup>	15/19	10, 4 ft	15/19
7 and 8	0.30	0.55	NR	49	20 + 5 <sup>h</sup> or 13 + 10 <sup>h</sup>	19/21	38 <sup>k</sup>	15/19	10, 4 ft	15/19

TABLE N1102.1.4 (R402.1.4)  
EQUIVALENT U-FACTORS\*

CLIMATE ZONE	FENESTRATION U-FACTOR	SKYLIGHT U-FACTOR	CEILING U-FACTOR	FRAME WALL U-FACTOR	MASS WALL U-FACTOR <sup>a</sup>	FLOOR U-FACTOR	BASEMENT WALL U-FACTOR	CRAWL SPACE WALL U-FACTOR
1	0.50	0.75	0.035	0.084	0.197	0.064	0.360	0.477
2	0.40	0.65	0.030	0.084	0.165	0.064	0.360	0.477
3	0.32	0.55	0.030	0.060	0.098	0.047	0.091 <sup>e</sup>	0.136
4 except Marine	0.32	0.55	0.026	0.060	0.098	0.047	0.059	0.065
5 and Marine 4	0.30	0.55	0.026	0.060	0.082	0.033	0.050	0.055
6	0.30	0.55	0.026	0.045	0.060	0.033	0.050	0.055
7 and 8	0.30	0.55	0.026	0.045	0.057	0.028	0.050	0.055

### REScheck

**\*UA**\_UA IS THE RECOGNIZED ACRONYM FOR COMPOSITE TRANSMITTANCE VALUE (U) TIMES THE SURFACE AREA (A). NOTED THESE 2 THINGS WE CAN CONTROL TO GENERATE A MORE EFFECTIVE THERMAL ENVELOPE. REScheck IS A SPREADSHEET THAT TAKES INSULATION R VALUES, WITH JUST A FEW QUALIFIERS THE USER IS ASKED FOR, AND GIVES US U-FACTORS AND UA TOTALS WITHOUT THE USER NEEDING A CALCULATOR.

**\*FREE AND SIMPLE**\_RESCHECK IS A DEPARTMENT OF ENERGY PRODUCT THAT EXISTS TO HELP US DO THIS STUFF. THERE IS AN ON-LINE AND DOWNLOADABLE VERSION. CHECK APPROPRIATE CODE COMPLIANCE VERSION (MAYBE A LITTLE BEHIND ON THIS). IT IS SIMPLE, NO REASON FOR INTIMIDATION. REMEMBER THIS IS A CODE COMPLIANCE TOOL ONLY. JUST SEARCH resCHECK.

**\*AS DESIGN TOOL**\_ONE CAN PLAY WITH R VALUE INPUTS AND AREAS AND COMPARE UA RESULTS SO EASILY.....

### R compliance BASED ON MIN 'R' VALUES BY COMPONENT

**\*FOOTNOTES**\_ONE REALLY HAS TO READ ALL FOOTNOTES THESE TABLES.

ALL THE 'DOUBLE NUMBER' SITUATIONS ARE EXPLAINED THERIN. AND THAT AT MINIMUM NEEDS TO BE UNDERSTOOD.

**\*FOUNDATIONS/WALLS/ROOFS**\_(c3.6-c3.15)(c6.16-c6.19)(c7.25-c7.27) THE COMPOSITE CONDITIONS EFFECTING THESE PRIME ASSEMBLIES ARE ADDRESSED IN THEIR RESPECTIVE CHAPTERS.

**\*GLAZING**\_SWITCHES TO A U-FACTOR REQUIREMENT AS EXPLAINED ABOVE.

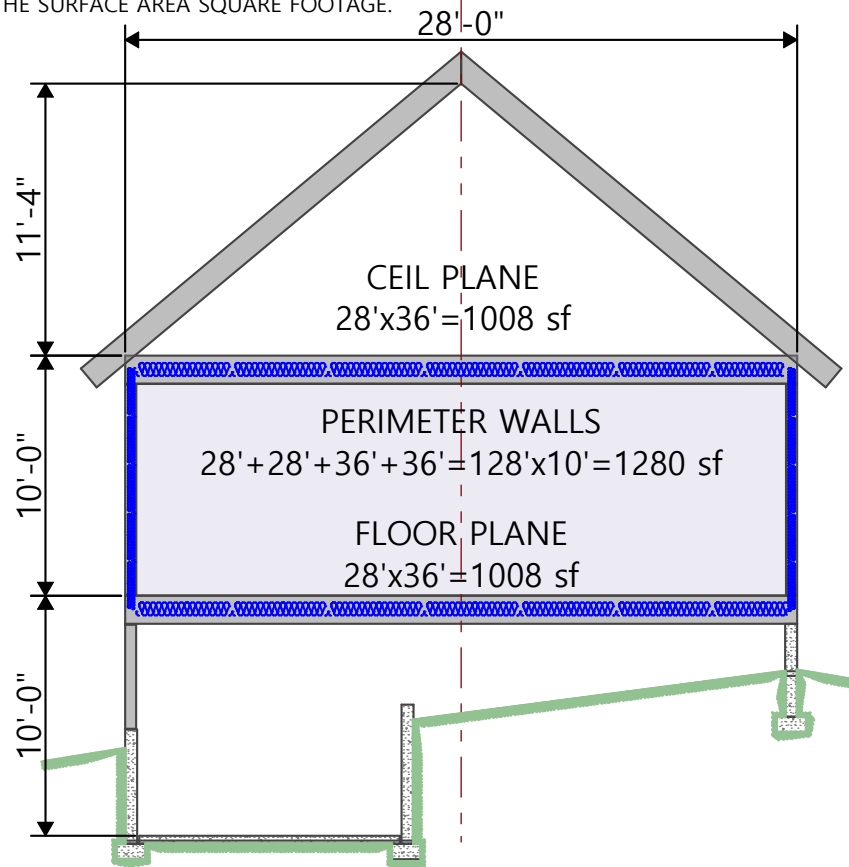
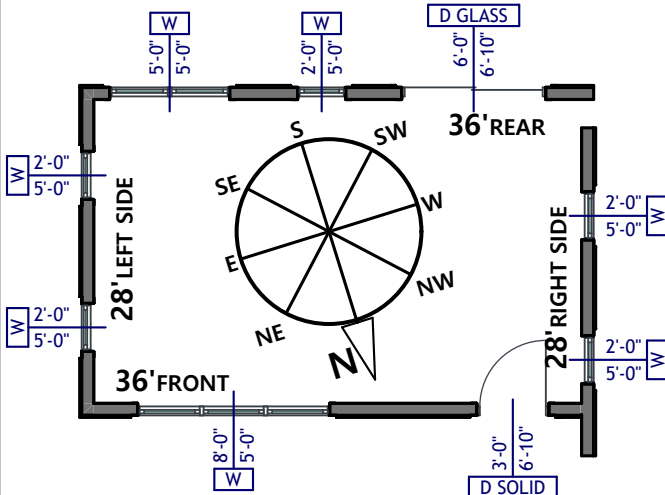
### U compliance BASED ON MAX 'U' VALUES BY ASSEMBLY

**\*ASSEMBLY VALUE**\_IF/WHEN USING THE U FACTOR COMPLIANCE METHOD THE APPLICANT BECOMES OBLIGED TO TALLY+VERIFY ALL ASSEMBLIES WITH ACCURATE TOTAL ASSEMBLY U VALUES. THIS CAN BE A BIT OF WORK.

**\*WHY DO THIS?**\_ASSEMBLY CALCULATIONS ARE A MORE ACCURATE WAY OF GETTING TO A REAL PROTECTION VALUE, AND SUBSEQUENTLY A MORE ACCURATE HEAT GAIN AND LOSS NUMBER. AND THE EXERCISE FORCES ONE TO UNDERSTAND THE COMPLEXITY OF ANY PROPOSED CONSTRUCTION. OUR HYGRO-THERMAL ASSEMBLIES ARE GETTING MORE COMPLICATED. COMPLEXITY ALWAYS COSTS MORE MONEY AND PRESENTS MORE OPPORTUNITY FOR PROBLEMS, HENCE THIS BECOMES AN OPPORTUNITY TO CHECK ALL CIRCUITS.

## SAMPLE PROJECT COMPARISON

\*REScheck\_THIS SIMPLE BOX (28' DEEP AND 36' LONG) HOUSE WILL BE CHECKED OUT USING REScheck UA METHOD. LETS SEE HOW IT ENDS UP. ALL THE SAME VALUES WILL BE INPUT FOR THE SMALLER THERMAL ENVELOPE VERSION [THIS PAGE] AND THE LARGER THERMAL ENVELOPE (NEXT PAGE). THE INTENT IS TO FIND THE UA PENALTY FOR INCREASING THE SURFACE AREA SQUARE FOOTAGE.



### NOTE ON ORIENTATION (AND HEAT GAIN)

\*BOTH CODE AND REScheck\_EXCEPTING THE SHGC FOR GLAZING IN ZONES 1-4, CODE AND REScheck TAKE HEAT GAIN OUT OF THEIR REQUIREMENTS SET. ALTHOUGH THERE IS AN ORIENTATION TAB IN THIS REScheck SAMPLE IT IS ONLY FUNCTIONING AS A REFERENCE.

\*HEAT GAIN\_AND ITS QUALIFIER-ORIENTATION TO THE SUN-ARE A VERY ESSENTIAL PART OF ALL HVAC LOAD CALCULATIONS.

### BASE UA CALCULATION

\*INPUT\_FOLLOWS CODE MINIMUM COMPONENT R VALUES. AND THE RESULT IS 1.6% BETTER THAN CODE. JUST AS IT SHOULD BE.

\*UA MAX\_REScheck SETS A MAX UA BASED ON CODE MINIMUM U VALUES COMBINED WITH THE AREAS FOR EACH COMPONENT PER USER INPUT. IT IS REALLY ONLY TESTING

### ADJUSTMENT UA CALCULATION

\*INCREASED INSULATION\_1" OF XPS (R-5) IS ADDED TO ALL EXTERIOR WALLS AND THE FLOOR PLANE AND AN ADDITIONAL 3" OF LOOSE INSULATION (R-11) ADDED TO THE CEILING PLANE. THE RESULT IS A UA OR 155 OR 26 BELOW THE CODE MINIMUM STANDARD ABOVE OF 181 REPRESENTING AN EFFICIENCY INCREASE OF 14%. REMEMBER THAT 14% REPRESENTS THE FULL THERMAL ENVELOPE.

\*PAY BACK\_A QUESTION THEN IS FIRST WHAT IS THE COST OF THAT ADDITIONAL R AND HOW LONG DOES IT TAKE TO GET THAT INVESTMENT BACK AT AN ENERGY SAVINGS OF 14% PER YEAR.??

### REScheck PERFORMANCE ALTERNATIVE

\*LIMITED VALUE\_REScheck's OTHER COMPLIANCE OPTION (OTHER THAN THE UA TRADE OFF METHOD) IS THE PERFORMANCE ALTERNATIVE THAT CONSIDERS THE EFFICIENCY OF THE BASIC HVAC EQUIPMENT SELECTED. IT HAS LIMITED VALUE AS A DECISION TOOL, AND NOT EXPERIMENTED WITH THIS PROJECT.

Component	Assembly	Orientation	Gross Area	Cavity Insulation R-Value	Continuous Insulation R-Value	U-Factor	UA	
Building								
1	Floor 1	All-Wood Joist/Truss O.	1008	#2	30.0	0.033	33	
2	Wall 1	Wood Frame, 16" o.c.	360	#2	20.0	0.059	18	
3	Window 1	Wood Frame Double P.	40	#2		0.3	12	
4	Door 1	Solid	21	#2		0.2	4	
5	Wall 2	Wood Frame, 16" o.c.	280	#2	20.0	0.059	15	
6	Window 2	Wood Frame Double P.	25	#2		0.3	8	
7	Wall 3	Wood Frame, 16" o.c.	360	#2	20.0	0.059	17	
8	Window 3	Wood Frame Double P.	35	#2		0.3	11	
9	Door 2	Glass	42	#2		0.3	13	
10	Wall 4	Wood Frame, 16" o.c.	280	#2	20.0	0.059	15	
11	Window 4	Wood Frame Double P.	25	#2		0.3	8	
12	Ceiling 1	Flat Ceiling or Scissor	1008	#2	49.0	0.026	26	
Compliance Method: UA Trade-Off							Max UA: 184	Your UA: 181
Compliance Method: UA Trade-Off							Max UA: 184	Your UA: 155

## SISTER SAMPLE PROJECT

\*REScheck\_SAME BOX DESIGN, SAME ORIENTATION, WITH A DIFFERENT ENVELOPE DESIGN. THE VALUE ENGINEERING WANTS TO WEIGH THE ADDITIONAL CONSTRUCTION COST AND ANNUAL ENERGY EXPENSE AGAINST THE VALUE OF AN ENCLOSED HVAC SYSTEM (WHETHER IN ATTIC OR CRAWL SPACE), THE VALUE OF CONDITIONED ATTIC STORAGE, AND A CONDITIONED WORK SPACE AS PART OF THE CRAWL. THIS EXERCISE CANNOT PUT HARD NUMBERS TO THIS, WHICH WOULD ULTIMATELY BE SMART. BUT CONSIDERATIONS CAN BE NOTED.

### THE ATTIC CLOSURE IS SIMPLER

\*SURFACE SQUARE FEET\_THIS ILLUSTRATION NOTES A 1008 SF AREA FOR THE FLAT CEILING PLANE AND A 1296 SF AREA FOR THE ROOF PLANE. A 22% GREATER SURFACE AREA AND 22% GREATER ENERGY PENALTY FOR THE ROOF COMPONENT. THAT PENALTY, ON A PERCENTAGE BASIS, GETS MUCH SMALLER WHEN FACTORED INTO THE ENTIRE ENVELOPE.

\*CONSTRUCTIONS\_(c7.24-c7.25) DO A GOOD JOB OF SUMMARIZING INSULATION CONSTRUCTION OPTIONS FOR THE ROOF PLANES

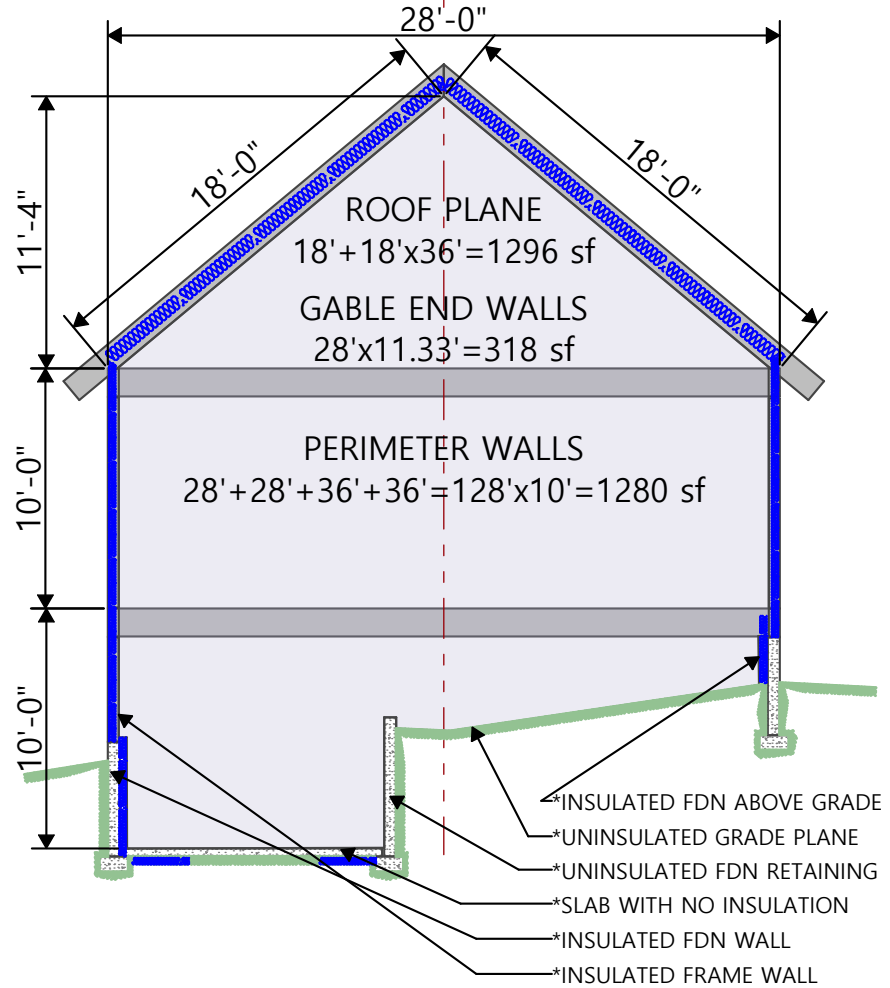
### THE CRAWL CLOSURE MAY NOT BE

\*THIS SAMPLE PROJECT\_SHOWS A PARTIAL CRAWL AND PARTIAL BASEMENT AND A SLOPED SITE. SOME COMPLICATIONS SHOW UP.

\*THE CLOSED CRAWL IDEA\_INVOLVES SEALING UP THE WHOLE SPACE AGAINST MOISTURE AND AIR LEAKAGE. IT ALSO INVOLVES THERMALLY PROTECTING IT AS THIS SPACE EFFECTIVELY BECOMES CONDITIONED.

**FYI: MAX UA for this 1008 sf sample project: goes down in colder climates? why**

- Zone 1a\_287
- Zone 2a\_261
- Zone 3a\_208
- Zone 4a\_204
- Zone 5a\_184
- Zone 6a\_167
- Zone 7\_162



## UA COMPARISONS

\*ADDING SURFACES\_WHEN USING THE REScheck TOOL EVERYTIME A NEW SURFACE IS ADDED THE PROGRAM INCREASES THE MAX UA NUMBER. KEEP IN MIND IT IS SEEKING ADEQUATE THERMAL PROTECTION ON A SURFACE AREA UNIT BASIS. IT IS NOT INTERESTED IN MANAGING SQUARE FOOTAGE.

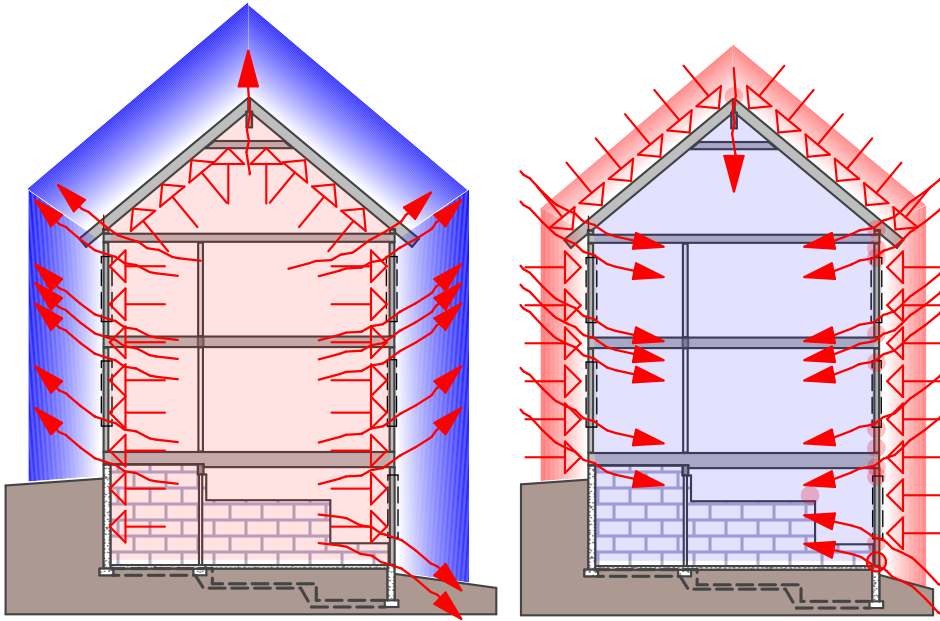
\*USING THE UA\_THIS EXPANDED THERMAL ENVELOPE HAS A MAX UA OF 291. THE MORE CONTAINED (c9.5) THERMAL ENVELOPE HAS A MAX UA OF 184. THIS COMPARISON ILLUSTRATES HOW SQUARE FOOTAGE MATTERS. ONE CAN PLUG THESE UA'S INTO THE BASE LOAD FORMULA AND TRANSLATE RESULTS INTO BTU'S. REGARDLESS OF DELTA T THIS SAME PROPORTIONAL RELATIONSHIP WILL EXIST. NOTE INCLUDED BELOW IS THE UA OF 348 FOR A FULL BASEMENT SUBSTITUTION FOR THE HYBRID CRAWL CONSTRUCTION ILLUSTRATED ABOVE.

\*MORE R\_IF ONE ADDS MORE R (LESS U) IN CONSISTENT LOCATIONS IN EACH OF THE THREE CONFIGURATIONS BEING COMPARED THE ABOVE CODE COMPLIANCE PERCENTAGE WILL RISE, THE ENERGY REQUIREMENT WILL DIMINISH, BUT THE PROPORTIONAL DIFFERENCE WILL REMAIN THE SAME. SQUARE FOOTAGE MATTERS.

Component	Assembly	Orientation	Gross Area of Shell Perimeter	cavity insulation U-Value	Continuous Insulation U-Value	U-Factor	UA	Wall Height (ft)	Depth Below Grade (ft)	Depth of Insulation (ft)	Depth Below Inside Grade (ft)
1	Floor 1	Sub-On-Grade Unles	92		10.0	0.738	67			2.5	
2	Crawl 1	Solid Concrete or Mas.	360	0.0	15.0	0.058	19	5.0	2.5	5.0	0.0
3	Crawl 2	Solid Concrete or Mas.	140	0.0	15.0	0.058	7	7.0	3.0	7.0	0.0
4	Crawl 3	Solid Concrete or Mas.	144	0.0	15.0	0.058	9	4.0	3.0	7.0	0.0
5	Crawl 4	Wood Frame	108	20.0	0.0	0.13	23	3.0	0.0	3.0	0.0
6	Wall 1	Wood Frame, 16" o.c.	360	20.0	0.0	0.059	6				
7	Window 1	Wood Frame Double P.	40			0.3	12				
8	Door 1	Solid	21			0.2	4				
9	Wall 2	Wood Frame, 16" o.c.	280	20.0	0.0	0.059	15				
10	Window 2	Wood Frame Double P.	25			0.3	6				
11	Wall 3	Wood Frame, 16" o.c.	360	20.0	0.0	0.059	17				
12	Window 3	Wood Frame Double P.	30			0.3	11				
13	Door 2	Glass	42			0.3	13				
14	Wall 4	Wood Frame, 16" o.c.	280	20.0	0.0	0.059	15				
15	Window 4	Wood Frame Double P.	25			0.3	6				
16	Wall 5	Wood Frame, 16" o.c.	159	20.0	0.0	0.059	9				
17	Wall 6	Wood Frame, 16" o.c.	159	20.0	0.0	0.059	9				
18	Ceiling 1	Cathedral Ceiling	1296	29.0	20.0	0.02	26				

\*THE HYBRID CRAWL BASEMENT IS FUSSY

\*FULL BASEMENT UA



### THE CONSTANT PROBLEM

**\*HOT TO COLD**\_DELTA T IS THE ENGINE THAT IS ALWAYS RUNNING. SO THERE IS SELDOM ANY RELIEF FROM THE HEAT LOSS OR HEAT GAIN CONTINUUM.

**\*CONDITION 1-THERMAL TRANSFER**\_BASED ON SURFACE SQUARE FOOTAGE AND R, U, OR UA) VALUE. ALL SURFACES INTERFACING TEMPERATURE DIFFERENTIALS ARE NEEDING THERMAL RESISTANCE TO LIMIT THERMAL TRANSFER.

**\*CONDITION 2-THERMAL LEAKS**\_ARE A SEPARATE BUT INTEGRATED PROBLEM AND MUST BE ADDRESSED IN ADDITION TO THE TRANSFER NOTED. THE WORKING TERM AS THE RESOLUTION TO LEAKS IS SEALING OR AIR SEALING THE INSULATED THERMAL BARRIER. AN OFT QUOTED AND EFFECTIVE ANALOGY TO THIS DEMAND IS THE WINTER FLEECE TYPE COAT. TO STAY WARM IT WANTS TO BE ZIPPED, AND TIGHT AT THE COLLAR AND SLEEVES (NO LEAKS). TO STAY WARM IT REALLY WANTS A AIR BLOCKING SHELL SO THE FLUFFY FLEECE INSULATION CAN BETTER DO ITS JOB. DITTO THE HOUSE. TAPE, CAULK, THE LEAKS, AND HAVE AN AIR BARRIER CONTINUOUSLY INSTALLED IN CONJUNCTION WITH THE INSULATION TO INCREASE ITS EFFECTIVENESS.

### TechNote

Building Air Tightness:  
Code Compliance & Air Sealing Overview

THIS IS A SHORT DOCUMENT SPONSORED BY THE ICC AND NAHB THAT DOES CONTAIN A GREAT 3D ILLUSTRATION OF AIR LEAKAGE LOCATION CANDIDATES.



THIS GUIDE SEEMS COMPREHENSIVE. GOVERNMENT SPONSORED PRESENTATIONS TEND TO BE REASONED. THEY ARE NOT SELLING ANYTHING.

## BSI-053: Just Right and Airtight

THE BUILDING SCIENCE CORPORATION ALSO KEEPS AN EYE ON WHATS REAL AND WHAT IS NOT. THIS 'INSIGHT' IS A MUST READ AS A MEANS OF MAINTAINING PERSPECTIVE ON WHAT THE SMART THING TO DO IS.

### SEALING REFERENCES

**\*AT LEFT**\_JUST A FEW RESOURCES FOR A QUICK COURSE IN AIR TIGHTNESS. THERE IS A MOUNTAIN OF DATA AVAILABLE. THESE RESOURCES WILL DO A MUCH BETTER JOB OF PRESENTATION THAN THIS PROJECT CAN. AS WITH ALL RESEARCH-BEWARE THOSE SELLING SOMETHING.

### INSPECTING TIGHTNESS

**\*KNOWLEDGE**\_KNOWING WHERE A HOME CHARACTERISTICALLY LEAKS IS A GREAT START.

**\*VISUAL INSPECTIONS**\_THAT KNOWLEDGE HELPS DIRECT A VISUAL INSPECTION. THESE CAN'T BE CURSORY. LEAKS CAN BE REAL TINY.

**\*BLOWER DOOR TESTING**\_WHEN PROPERLY EMPLOYED THE BLOWER DOOR TEST IS A GREAT BACKUP TOOL THAT EITHER SALUTES A SUCCESSFUL HOME SEALING, OR TELLS US WE STILL GOT SOME LEAKS TO PLUG.

**\*ACCEPTABLE PARAMETERS**\_THE CODE HAS GENERATED 2 ACCEPTABLE LEAKAGE LIMITS-BASED ON CLIMATE ZONE. SOME ACCEPT THESE LEVELS AS REASONABLE AND OTHERS DO NOT. IF ONE WANTS TO GET DIZZY THERE IS ANOTHER MOUNTAIN OF TECHNICAL OPINION AND DATA READILY AVAILABLE TO RESEARCH.

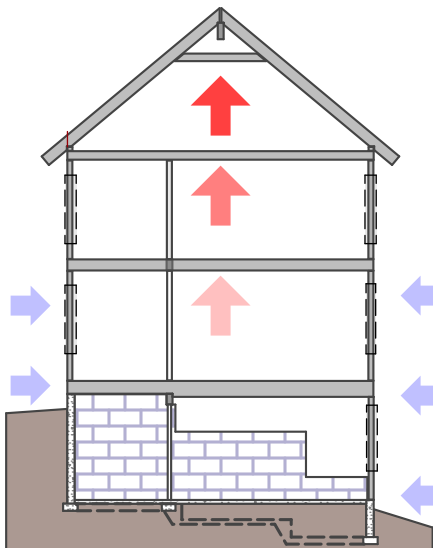
### STACK EFFECT

**\*MOTHER NATURE**\_WARMER AIR RISES BECAUSE IT IS LIGHTER THAN COOLER AIR. THE HOT AIR BALLOON IDEA. WHEN THAT WARMER AIR ESCAPES TO THE OUTSIDE THE PRESSURE CHANGE CREATED WANTS TO SUCK IN COOLER AIR. THE MANY READILY AVAILABLE IMAGES ILLUSTRATING THIS STACK EFFECT ARE SIMILAR TO THE ONE AT LEFT AND SHOW WARMER AIR ESCAPING HIGHER IN THE HOUSE GEOMETRY WITH COOLER AIR ENTERING LOWER IN THE HOUSE GEOMETRY.

**\*EXFILTRATION**\_IS THE TERM USED DENOTING THE EXITING WARMER AIR. THAT EXIT IS CONDITIONAL ON THE OUTSIDE AIR BEING COOLER (HOT TO COLD), AND THEREFORE THE STACK EFFECT IS COOL TO COLD WEATHER CONDITIONAL.

**\*INFILTRATION**\_IS THE TERM DENOTING THE ENTRY OF COOLER AIR.

**\*TRY AS WE MIGHT**\_TO GET A HOME TIGHT, IT IS NOT REALISTIC TO EXPECT A HOME CONSTRUCTION TO BE 100% AIR TIGHT. AND IN FACT WE DON'T WANT THEM THAT TIGHT.



### FRESH AIR/MAKE UP AIR

**\*THE CATCH 22**\_THE 100% TIGHT HOUSE (WERE IT ACHIEVEABLE) HAS A FATAL FLAW. A HOME NEEDS A CERTAIN AMOUNT OF FRESH (HOPEFULLY) AIR, aka MAKE UP AIR. PRESSURE NEEDS TO BE BALANCED, COMBUSTION APPLIANCES AND FIREPLACES NEED COMBUSTION AIR, AND RECYCLED 'STAGNANT' AIR BECOMES A HEALTH RISK AND NEEDS (HOPEFULLY) HEALTHY STUFF FROM OUTSIDE.

**\*SO**\_VENTILATION, aka MAKE UP AIR, IS NECESSARY AND CODE REQUIRED. THESE REQUIREMENTS ARE IN THE MECHANICAL SECTION OF THE CODE. THERE ARE A FEW DIFFERENT STRATEGIES FOR BRINGING THIS MAKE UP AIR INTO THE HOUSE, AND (ALSO) A LITTLE OUTSIDE THE SCOPE OF THIS GUIDE. HVAC CONTRACTORS AND OR ENERGY CONSULTANTS ARE TYPICALLY GOOD RESOURCES. FOR REQUIREMENTS AND BEST METHODS.





**\*THIS PROJECT\_DUCTING OVERVIEW NOTES ARE INCLUDED THIS CHAPTER BECAUSE THE DUCTED HVAC SYSTEM HAS BEEN SELECTED AS THE DEFAULT THIS PROJECT. THE BUILDING SHELL AND STRUCTURE MUST ALLOW SPACE FOR THE DUCTWORK. DUCTWORK SIZING/SPACE ALLOWANCE IS GENERATED FROM SOME RULES OF THUMB AND CFM CONSIDERATIONS WHICH RESULTS IN DUCT SIZING. SEE (c9.12). THIS IS INCLUDED AS AN AWARENESS EXERCISE. IT IS NOT POSSIBLE TO DESIGN ANY HVAC PACKAGE WITHOUT SPECIFIC SITE AND ORIENTATION DATA.**

### N1103.3 (R403.3) Ducts.

Ducts and air handlers shall be installed in accordance with Sections N1103.3.1 through N1103.3.8.

#### N1103.3.1 (R403.3.1) Insulation (Prescriptive).

Supply and return ducts in attics shall be insulated to an R-value of not less than R-8 for ducts 3 inches (76 mm) in diameter and larger and not less than R-6 for ducts smaller than 3 inches (76 mm) in diameter. Supply and return ducts in other portions of the *building* shall be insulated to not less than R-6 for ducts 3 inches (76 mm) in diameter and to not less than R-4.2 for ducts smaller than 3 inches (76.2 mm) in diameter.

**Exception:** Ducts or portions thereof located completely inside the *building thermal envelope*.

#### N1103.3.3 (R403.3.3) Duct testing (Mandatory).

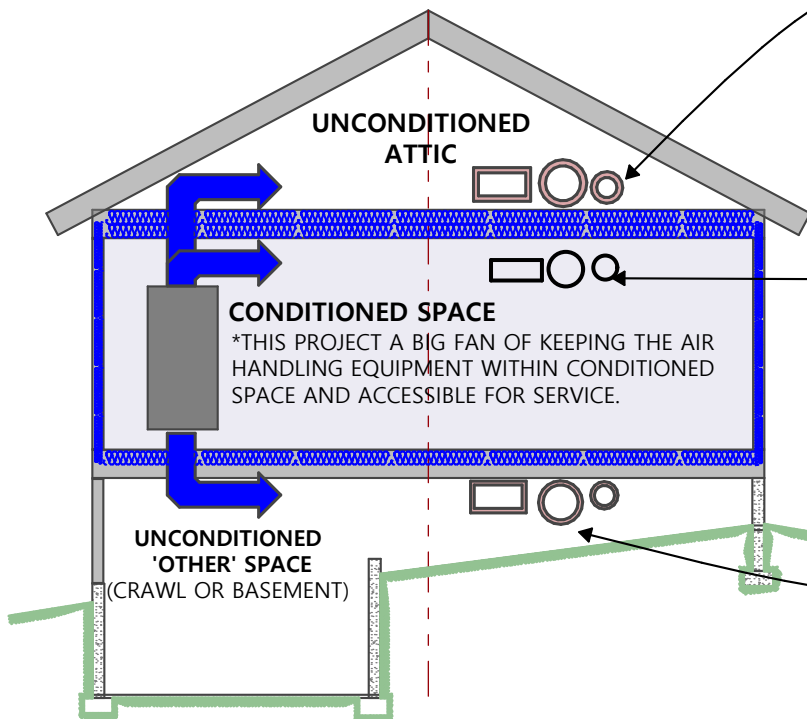
Ducts shall be pressure tested to determine air leakage by one of the following methods:

1. Rough-in test: Total leakage shall be measured with a pressure differential of 0.1 inch w.g. (25 Pa) across the system, including the manufacturer's air handler enclosure if installed at the time of the test. Registers shall be taped or otherwise sealed during the test.
2. Postconstruction test: Total leakage shall be measured with a pressure differential of 0.1 inch w.g. (25 Pa) across the entire system, including the manufacturer's air handler enclosure. Registers shall be taped or otherwise sealed during the test.

#### Exceptions:

1. A duct air-leakage test shall not be required where the ducts and air handlers are located entirely within the *building thermal envelope*.
2. A duct air-leakage test shall not be required for ducts serving heat or energy recovery ventilators that are not integrated with ducts serving heating or cooling systems.

A written report of the results of the test shall be signed by the party conducting the test and provided to the *building official*.



#### FOR DUCTS IN NON CONDITIONED ATTIC SPACES

- \*R-8 DUCTS 3"ID AND GREATER
- \*R-6 DUCTS SMALLER THAN 3"ID
- \*DUCT LEAKAGE TEST REQUIRED
- \*IT IS EASY TO RUN DUCTS UP HERE AS THERE ARE NO PHYSICAL BARRIERS EXCEPTING TRUSS WEBS. ROUND FLEX DUCTS ARE AN INSTALLATION SNAP. BURTING DUCTS UP HERE IS DOABLE AND OFFERS MUCH BETTER PERFORMANCE.SEE (c9.11). THINK ABOUT DUCTS TRYING TO DELIVER 65° COOLING IN A 120° ATTIC SPACE. IT DOESN'T COMPUTE.

#### FOR DUCTS IN CONDITIONED SPACE

- \*NOT DOING THIS IS DUMB.
- \*NO INSULATION REQUIRED
- \*DUCT LEAKAGE TEST NOT REQUIRED
- \*\*LEAKY DUCTS- REALLY ANY DUCT INEFFICIENCY- ARE PERMITTED BUT NOT ADVISED. NEW CONDITIONED AIR WILL STAY WITHIN THE THERMAL ENVELOPE WHICH IS GOOD, BUT IT NOT GETTING DELIVERED TO THE INTENDED DISCHARGE POINT EFFICIENTLY STILL MAKES THE SYSTEM HAVE TO WORK HARDER.

#### FOR DUCTS IN NON CONDITIONED OTHER SPACES

- \*R-6 DUCTS 3"ID AND GREATER
- \*R-4.2 DUCTS SMALLER THAN 3"ID
- \*DUCT LEAKAGE TEST REQUIRED
- \*\*THE UNCONDITIONED CRAWL SPACE (OR BASEMENT) MAINTAINS A SLIGHTLY ADJUSTED OUTSIDE TEMPERATURE. THE DUCTWORK'S DELIVERY TEMPERATURE IS FIGHTING THAT CRAWL SPACE TEMPERATURE. IN WINTER MONTHS THIS IS A DRAG ON HEAT DELIVERY. COOLING MONTHS ACTUALLY HAVE A DEW POINT PROBLEM WITH PRETTY SIGNIFICANT AMOUNTS OF MOISTURE COLLECTING ON THE DUCTWORK.

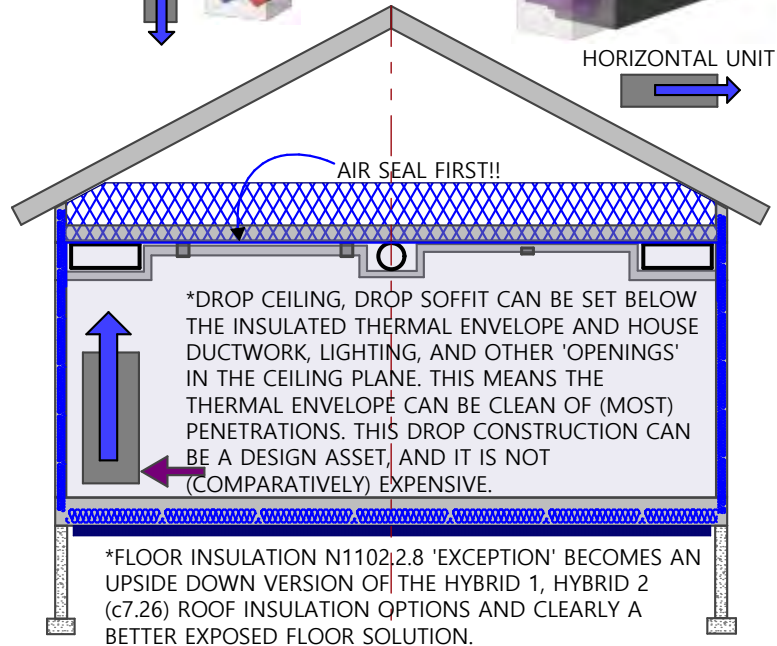
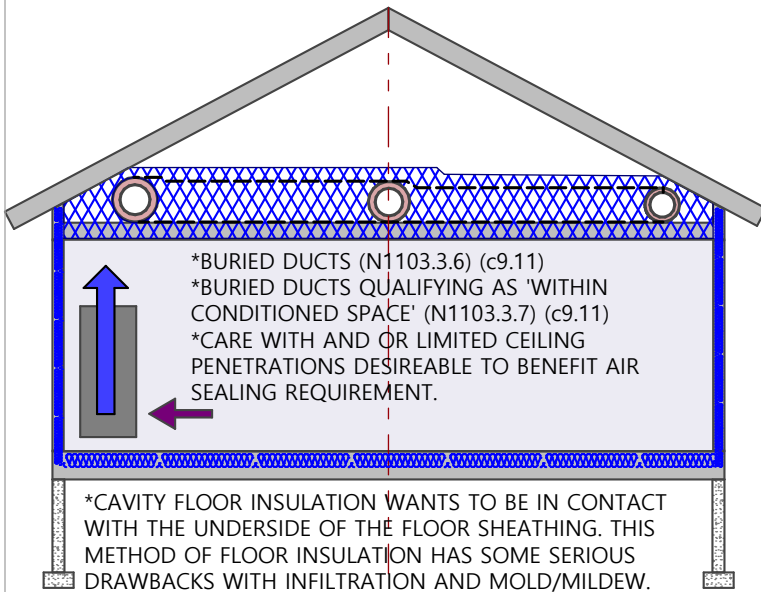
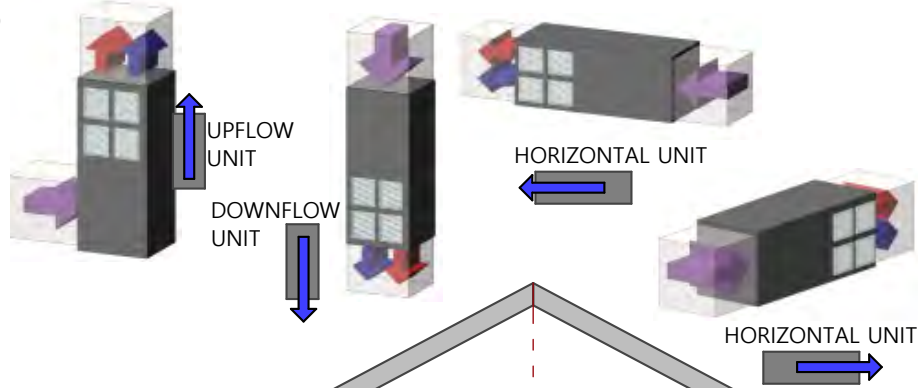
**\*DUCT SIZE, GEOMETRY AND LAYOUT\_(c9.12)** A FEW COMMENTS ON DUCTING ARE MENTIONED. THIS SCHEMATIC IS APPROPRIATE TO POINTING OUT ONE CONDITION WITH DUCT GEOMETRY. FOR EXAMPLE A 20" ROUND MAIN SUPPLY OR RETURN DUCT ARE POSSIBLE TO RUN IN THE OPEN AREAS DEPICTED IN THIS CRAWL AND ATTIC SPACES. RUNNING THAT SAME 20" ROUND DUCT WITHIN THE MAIN LEVEL CONDITIONED SPACE HOWEVER CAN BE A REAL PHYSICAL PROBLEM. A RECTANGULAR DUCT DELIVERING THE SAME AIR IS BETTER SUITED TO FIT- FOR EXAMPLE A SOFFIT SITUATION WHERE A WIDER AND NOT SO HIGH GEOMETRY IS BEST.

# THERMAL ENVELOPE c9.10 CONDITIONED SPACE DUCTING OPTIONS

## INTRO TO AIR HANDLER SPACE ALLOCATION (d8.15,d8.16)

\*HELPFUL TO REVIEW THOSE SCHEMATICS WHEN CONSIDERING THE BELOW

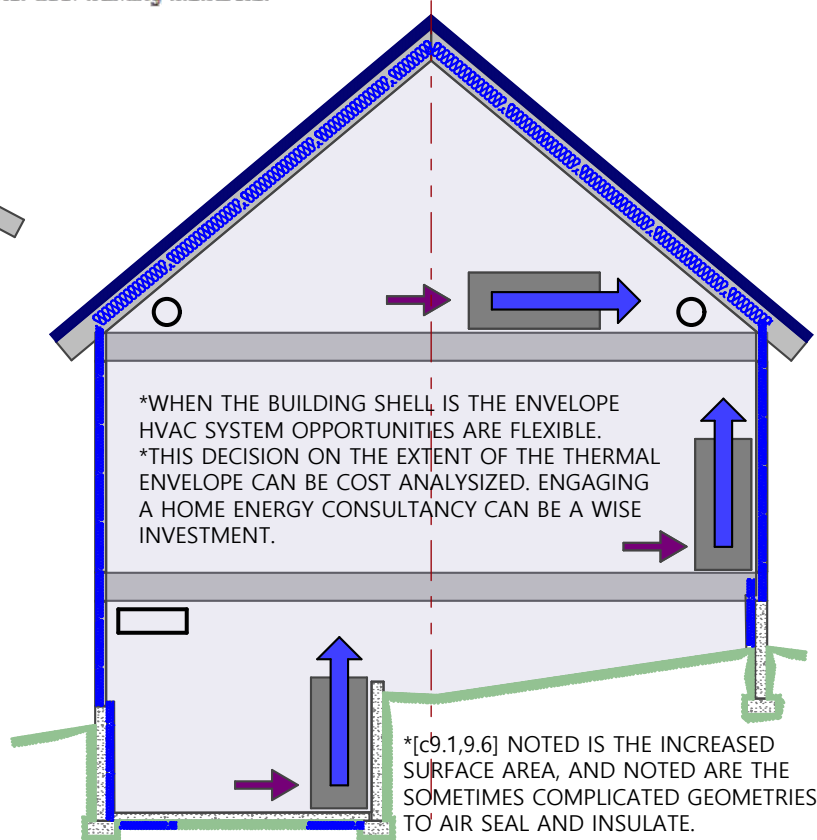
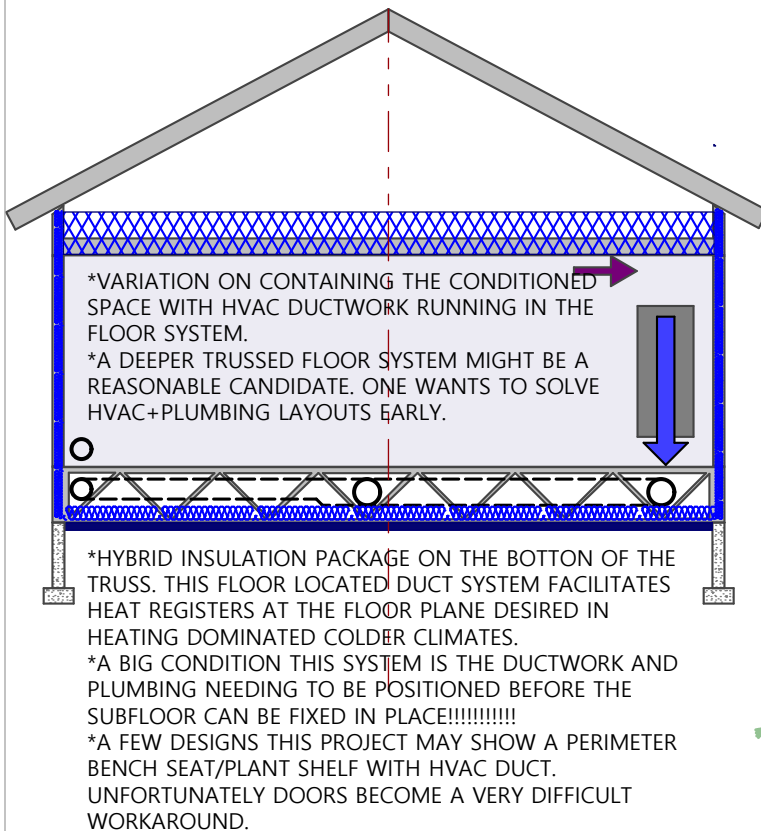
\*AIR HANDLERS AND DUCTS HAVE TO BE IN SYNC. THERE IS A SUPPLY SIDE AND A RETURN SIDE TO THE UNIT AND TO THE DUCT SYSTEM SERVING THE UNIT. SO THERE ARE CONDITIONS. DUCT SYSTEMS ARE -OF NECESSITY- CUSTOMIZED TO SUIT.



### N1102.2.8 (R402.2.8) Floors.

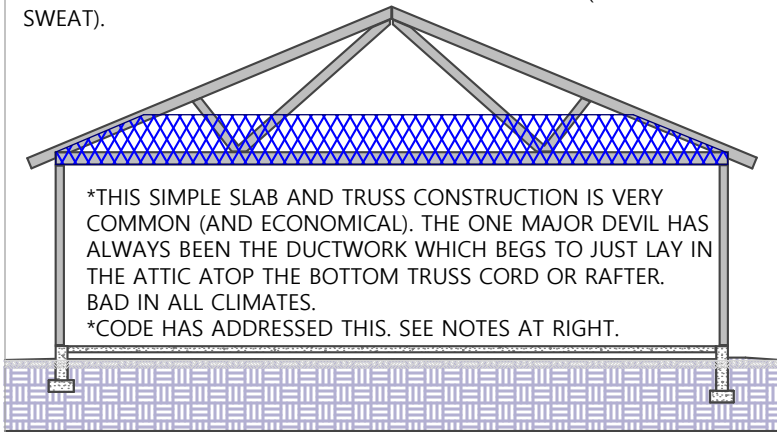
Floor framing-cavity insulation shall be installed to maintain permanent contact with the underside of the subfloor decking.

**Exception:** As an alternative, the floor framing-cavity insulation shall be in contact with the topside of sheathing or continuous insulation installed on the bottom side of floor framing where combined with insulation that meets or exceeds the minimum wood frame wall R-value in Table N1102.1.2 and that extends from the bottom to the top of all perimeter floor framing members.

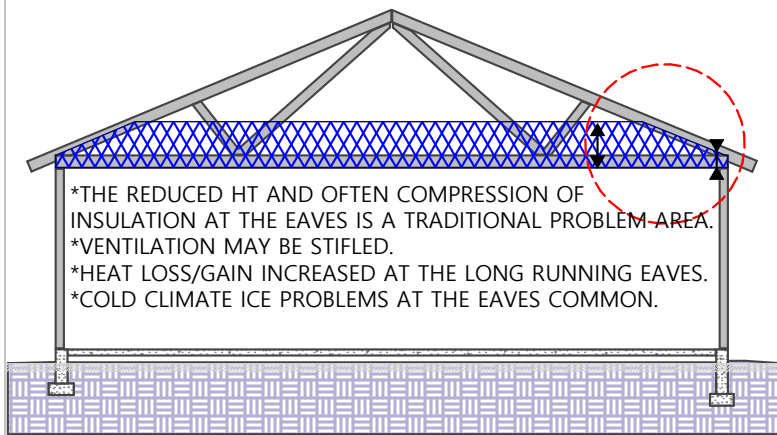


### OVERVIEW ON CEILING INSULATION

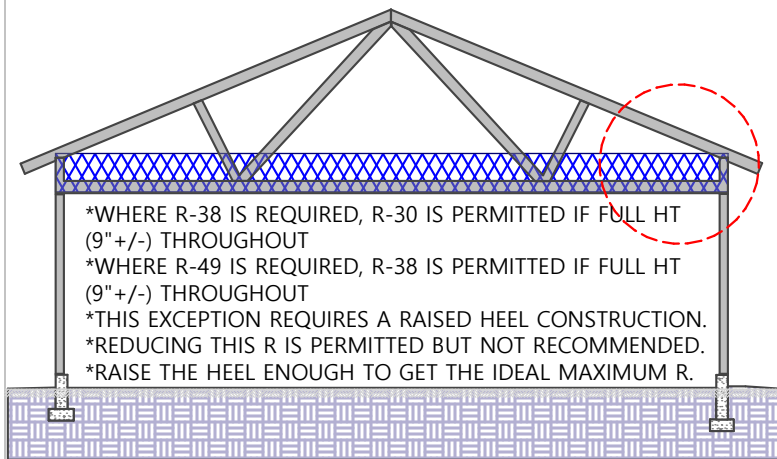
\*BUILDING SCIENCE CORP OFFERS A RELAYED ARTICLE ON BURIED DUCTWORK IN CEILINGS TITLED 'INSIGHT-NO SWEAT' (OR BSI-094: NO SWEAT).



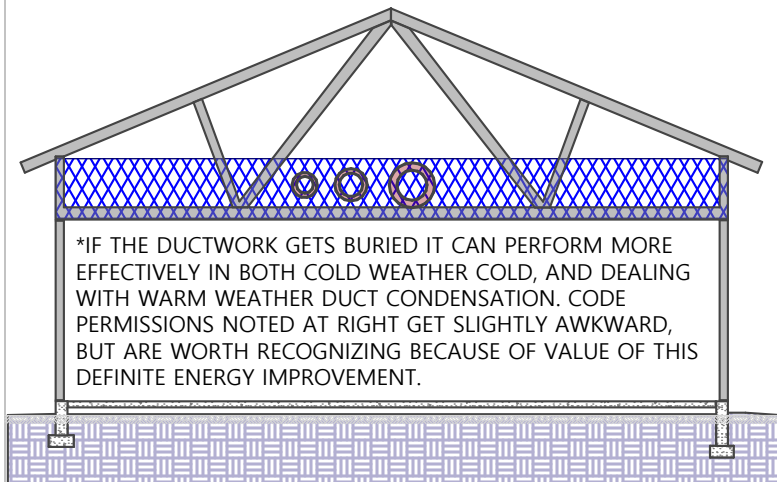
\*THIS SIMPLE SLAB AND TRUSS CONSTRUCTION IS VERY COMMON (AND ECONOMICAL). THE ONE MAJOR DEVIL HAS ALWAYS BEEN THE DUCTWORK WHICH BEGS TO JUST LAY IN THE ATTIC ATOP THE BOTTOM TRUSS CORD OR RAFTER. BAD IN ALL CLIMATES.  
\*CODE HAS ADDRESSED THIS. SEE NOTES AT RIGHT.



\*THE REDUCED HT AND OFTEN COMPRESSION OF INSULATION AT THE EAVES IS A TRADITIONAL PROBLEM AREA.  
\*VENTILATION MAY BE STIFLED.  
\*HEAT LOSS/GAIN INCREASED AT THE LONG RUNNING EAVES.  
\*COLD CLIMATE ICE PROBLEMS AT THE EAVES COMMON.

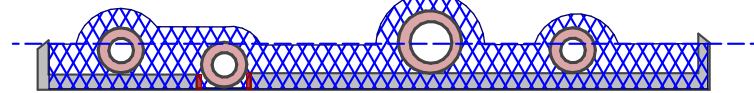


\*WHERE R-38 IS REQUIRED, R-30 IS PERMITTED IF FULL HT (9" +/-) THROUGHOUT  
\*WHERE R-49 IS REQUIRED, R-38 IS PERMITTED IF FULL HT (9" +/-) THROUGHOUT  
\*THIS EXCEPTION REQUIRES A RAISED HEEL CONSTRUCTION.  
\*REDUCING THIS R IS PERMITTED BUT NOT RECOMMENDED.  
\*RAISE THE HEEL ENOUGH TO GET THE IDEAL MAXIMUM R.



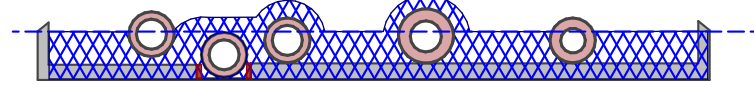
\*IF THE DUCTWORK GETS BURIED IT CAN PERFORM MORE EFFECTIVELY IN BOTH COLD WEATHER COLD, AND DEALING WITH WARM WEATHER DUCT CONDENSATION. CODE PERMISSIONS NOTED AT RIGHT GET SLIGHTLY AWKWARD, BUT ARE WORTH RECOGNIZING BECAUSE OF VALUE OF THIS DEFINITE ENERGY IMPROVEMENT.

### BURIED DUCTS IN THE ATTIC



#### N1103.3.6 DUCTS BURIED WITHIN CEILING INSULATION

\*FOR ZONES 1-3 R-30 OR R-38 IS THE BASELINE REQUIREMENT. THE R-13 INSULATED DUCTS MUST BE FULLY BURIED. THE 'COVER' INSULATION IS NOT SPECIFIED.



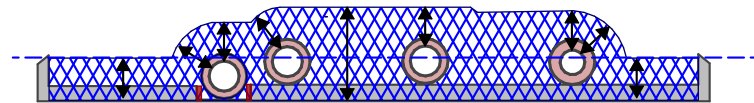
#### N1103.3.6 DUCTS BURIED WITHIN CEILING INSULATION

\*FOR ZONES 4-8 R-38 OR R-49 IS THE BASELINE REQUIREMENT. THE R-8 INSULATED DUCTS MUST HAVE AN R-19 BELOW, OR ABOVE, OR PRORTIONED AS SELECTED ABOVE AND BELOW.

#### N1103.3.6.1 EFFECTIVE R VALUE OF DEEPLY BURIED DUCTS

\*STATES THAT IF DUCTS ARE FULLY BURIED WITH 3.5" MIN OF INSULATION ABOVE, THEY WILL HAVE ACHIEVED AN EFFECTIVE R-25 FOR PURPOSES OF SIMULATED ENERGY PERFORMANCE ANALYSIS (AND HEAT GAIN/LOSS CALCS).

\*THIS WOULD NOT INCLUDE THE PERMITTED ZONE 4-8 INSULATED DUCT SITTING ABOVE THE BASELINE PLANE-WHICH IS A QUESTIONABLE TACTIC TO BEGIN WITH.



#### N1103.3.7 (BURIED) DUCTS LOCATED IN CONDITIONED SPACE

\*CONDITIONED SPACE IS REQUIRED TO HAVE A SEALED THERMAL BARRIER 'ENVELOPE'. BURIED DUCTS HAVE THE THERMAL BARRIER BUT ARE OUTSIDE THE SEALED AIR BARRIER. SO CONDITONS EXIST FOR THESE BURIED DUCTS TO BE CLASSIFIED AS BEING INSIDE THE THERMAL ENVELOPE-IN CONDITIONED SPACE. THIS IS IMPORTANT BECAUSE HVAC SYSTEMS LOCATED WITHIN CONDITIONED SPACE BENEFIT GREATLY IN HEAT GAIN/LOSS CALCULATIONS WHICH RESULT IN SMALLER MORE EFFICIENT EQUIPMT

\*THE AIR HANDLER MUST BE WITHIN CONDITIONED SPACE- SO IT EITHER MUST BE LOCATED BELOW THE ATTIC PLANE OR CONSTRUCTED IN AN ATTIC "TENT" (HVAC ROOM) WHICH IS VIABLE IN LARGE PROJECTS WITH BIGGER ATTIC VOLUMES, BUT HARDLY PRACTICAL/POSSIBLE IN SMALL TRUSS ROOF CONSTRUCTIONS.

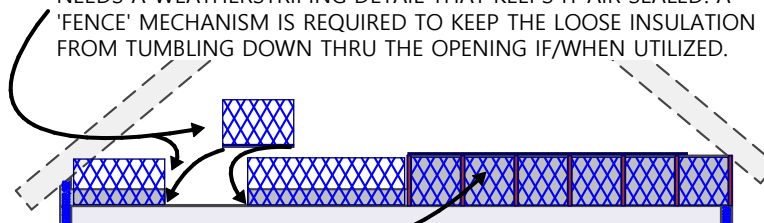
\*THE CODE PRESCRIBED R VALUE MUST BE MAINTAINED ABOVE ALL DUCTS.

\*DUCT LEAKAGE TESTING REQUIRED AND IS SIGNIFICANTLY MORE STRINGENT.

#### N1102.2.4 ATTIC ACCESS HATCH

\*THIS DESIGN SCENARIO-WITH DEEP INSULATION AND POSSIBLE BURIED DUCTS-SAYS THE ATTIC SPACE WILL NOT BE USED FOR STORAGE. THE AIR HANDLER IS LOCATED ON THE FLOOR BELOW, AND ACCESS IS ESSENTIALLY NOT USE REQUIRED, ONLY CODE REQUIRED.

\*THE INSULATION ABOVE THE HATCH OPNG HAS TO MAINTAIN THE SAME INSULATION VALUE AS THE CEILING PLANE, AND IT NEEDS A WEATHERSTRIPING DETAIL THAT KEEPS IT AIR SEALED. A 'FENCE' MECHANISM IS REQUIRED TO KEEP THE LOOSE INSULATION FROM TUMBLING DOWN THRU THE OPENING IF/WHEN UTILIZED.



#### OTHER SITUATIONS

\*(d6.10, a7) OTHER CONDITIONS (USUALLY WITHOUT DUCTS) CAN INSTALL FULL R DEPTH LOOSE INSULATION WITHIN A CEILING STRUCTURAL DEPTH, PUT A SUBFLOOR ON TOP, AND USE AN ATTIC FLOOR WITH PULL DOWN STAIR AS REASONABLE STORAGE. THE PULL DN STAIR OPENING IS SUBJECT TO THE SAME REQUIREMENT.

## HVAC DESIGN

**\*RULES OF THUMB THAT ARE DANGEROUS BUT USEFUL**\_ALL HVAC DESIGN IS REQUIRED TO BE CALCULATED USING THE MANUAL 'J' \_\_\_\_\_. THE THEORY IS THAT HEAT GAIN AND LOSS CALCULATIONS WOULD BE RESPONSIBLE AND ACCURATE, WHICH WOULD DIRECTLY RESULT IN EFFICIENT EQUIPMENT SELECTIONS. THE GENERIC BAD RAP ON RULES OF THUMB IS THAT EQUIPMENT GETS OVERSIZED TO BE ABSOLUTELY SURE THERE IS ENOUGH HEATING AND COOLING TO ADDRESS THE MOST EXTREME SITUATIONS. THE COOLING SIDE IS THE PRIMARY TARGET HERE AS OVERSIZED EQUIPMENT (TONS) WILL RUN INEFFICIENTLY AND LESS EFFECTIVELY THAN PROPERLY SIZED EQUIPMENT. THIS IS A PROVEN REALITY. THE MANUAL 'J' DOES NOT RELY ON RULES OF THUMB. WITH CORRECT AND CAREFUL INPUT IT WILL GENERATE HOUSE AND LOCATION SPECIFIC HEAT GAIN/LOSS AND SOLAR GAIN NUMBERS.

**\*RULES OF THUMB THIS SHEET**\_THIS SHEET HAS A RULE OF THUMB CHART THAT HAS ONE PURPOSE AND ONE BENEFIT. THE PURPOSE IS TO PROVIDE THIS PROJECT WITH SOME PARAMETERS FOR THE SUPPLY AND RETURN DUCT SIZES SO THAT WHEN A STRATEGY FOR A DUCTWORK LAYOUT IS POSSIBLE, PROPER SPACE WILL HAVE BEEN ALLOWED FOR THAT DUCTWORK. THE OPPORTUNITY OF THIS RULE OF THUMB CHARTING IS TO INFORM A LITTLE ABOUT THE RANGE OF VALUES IN THESE RULES OF THUMB AND THE REASONS FOR THEM.

## THIS PROJECTS' IN HOUSE DUCT CHART

**\*DOMINATION OF COOLING IN THIS DISCUSSION**\_WHEN FORCED AIR SYSTEMS ARE MANAGING COOLING AND HEATING IT IS MORE COMMON FOR THE DUCTWORK REQUIRED TO NEED TO BE LARGER FOR THE COOLING CYCLE. THIS IS OFTEN TRUE EVEN IN COLDER CLIMATES. BUT NOTE IT IS NOT ALWAYS THE CASE AND CERTAINLY NOT THE CASE WHEN HEATING ONLY IS BEING PROVIDED BY THE FORCED AIR SYSTEM. THIS IN HOUSE CHART BELOW USES COOLING IN TONS AS THE DUCT SIZE DETERMINANT.

**\*#1 RULE OF THUMB**\_HOW MANY SQUARE FEET OF LIVING SPACE CAN 1 TON OF AIR CONDITIONING HANDLE?

**\*MOST QUOTED RULE OF THUMB**\_400 SF, OR 600 SF. QUALIFIED HVAC FOLKS MIGHT SAY THE RANGE IS FROM 350 SF TO 2000 SF, BASED ON THE CLIMATE ZONE BUT MORE IMPORTANTLY ON THE GEOMETRY AND QUALITY OF THE THERMAL ENVELOPE.

**\*#2 RULE OF THUMB**\_HOW MANY CFM IS BEST TO DELIVER THAT TONAGE THROUGHOUT THE DUCT SYSTEM?

**\*MOST QUOTED RULE OF THUMB**\_400 CFM PER TON. AND THIS SEEMS A VIABLE RULE OF THUMB TO USE. OTHER ACCEPTED NORMS ARE HUMID AIR IS BETTER DELIVERED AT SLOWER RATES. 350 CFM OFTEN QUOTED. AND HEAT PUMP SYSTEMS PERFORM MORE EFFICIENTLY AT 450 OR 500 CFM. THIS PREFERRED CFM DELIVERY IS A BEST DESIGN TO EQUIPMENT SELECTION SEQUENCE.

**\*CFM IS THE ANSWER BEING SOUGHT**\_THE CFM (CUBIC FEET PER MINUTE) DICTATES THE DUCT SIZE. THAT SIMPLE. THE CFM PER TON THINKING ASSUMES THE COOLING SIDE IS DICTATING THE LARGER CFM AND THEREFORE DUCT SIZE. SEE NOTE ABOVE.

**\*SF PER TON 'YIELD' IS ESSENTIALLY AN EFFICIENCY RECOGNITION-HIGHER IS BETTER. SEE GLIB COMMENTS BELOW CHART.**

HOUSE SF	400 sf	600 sf	675 sf	750 sf	1000 sf	400 sf/TON	round flex	rectangular		
1000 SF	2.5 tons	2 tons	1.5 tons	1.5 tons	1 ton	600 cfm	14"dia	8" x 18"	10" x 14"	12" x 12"
1250 SF	3.5 tons	2.5 tons	2 tons	2 tons	1.5 tons	800 cfm	16"dia	8" x 22"	10" x 16"	12" x 14"
1500 SF	4 tons	2.5 tons	2.5 tons	2 tons	1.5 tons	1000 cfm	16"dia	8" x 26"	10" x 16"	12" x 18"
1750 SF	5 tons	3 tons	3 tons	2.5 tons	2 tons	1200 cfm	17"dia	8" x 30"	10" x 22"	12" x 20"
2000 SF	5 tons	3.5 tons	3 tons	3 tons	2 tons	1200 cfm	17"dia	8" x 30"	10" x 22"	12" x 20"
2250 SF	2 UNITS	4 tons	3.5 tons	3 tons	2.5 tons	1400 cfm	18"dia	8" x 34"	10" x 22"	12" x 20"
2500 SF	2 UNITS	5 tons	4 tons	3.5 tons	2.5 tons	1600 cfm	20"dia	8" x 40"	10" x 30"	12" x 24"

**\*400 SF**\_EITHER SLOPPY HVAC DESIGN OR SLOPPY HOME DESIGN.

**\*600 SF**\_THE ACCEPTABLE INEFFICIENT CATEGORY.

**\*675 SF**\_USED THIS PROJECT AS A COMPROMISE BETWEEN OK AND GOOD

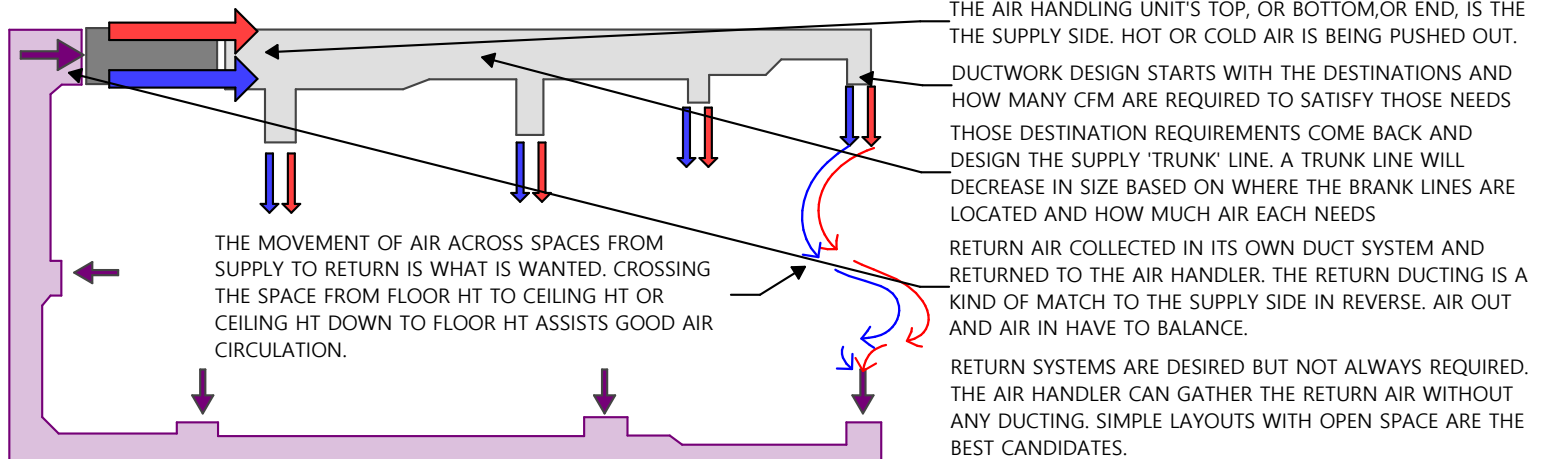
**\*750 SF**\_ENERGY STAR PERFORMANCE SHOULD GET HERE.

**\*1000 SF**\_REPRESENTS A THOUGHTFUL HOME AND HVAC DESIGN.

**\*HOUSE SF DIVIDED BY THE 675 SF PER TON EQUALS THE AC UNIT IN TONS, AND THEN DIVIDED BY THE 400 CFM PER TON TO GET THE UNIT'S CFM REQUIREMENT. THE MAIN SUPPLY AND RETURN SIZE IS BASED ON THAT CFM NUMBER.**

**\*LOTS OF ROOM FOR ERROR USING THESE RULES OF THUMB. EXACT SITE CONDITIONS, ORIENTATION AND THE MANUAL J,D,S CALCULATIONS NEEDED FOR REAL DESIGN.**

**\*SYSTEM SCHEMATIC IN A PLAN VIEW**\_SCHEMATICS IN d8.16, c9.9, c9.10 SHOW PROFILE SECTIONS THAT ARE ILLUSTRATING THE FLOOR TO FLOOR CONDITIONS A SYSTEM IS HAVING TO DEAL WITH. THOSE PROFILE CANNOT REALLY SHOW DUCT DELIVERY LAYOUTS. THIS SCHEMATIC IS USING A PLAN FORMAT TO MAKE A FEW GENERAL POINTS ABOUT DUCTWORK IN PLAN. CONVERSELY THIS SCHEMATIC CANNOT SHOW THE VERTICAL CONDITIONS DUCTWORK MAY ENCOUNTER.



**TABLE N1102.1.2 (R402.1.2) INSULATION AND FENESTRATION REQUIREMENTS BY COMPONENT<sup>a</sup>**

CLIMATE ZONE	FENESTRATION U-FACTOR <sup>b</sup>	SKYLIGHT <sup>b</sup> U-FACTOR	GLAZED FENESTRATION SHGC <sup>b, e</sup>	CEILING R-VALUE	WOOD FRAME WALL R-VALUE	MASS WALL R-VALUE <sup>i</sup>	FLOOR R-VALUE	BASEMENT <sup>c</sup> WALL R-VALUE	SLAB <sup>d</sup> R-VALUE & DEPTH	CRAWL SPACE <sup>e</sup> WALL R-VALUE
1	NR	0.75	0.25	30	13	3/4	13	0	0	0
2	0.40	0.65	0.25	38	13	4/6	13	0	0	0
3	0.35	0.55	0.25	38	20 or 13 + 5 <sup>h</sup>	8/13	19	5/13 <sup>f</sup>	0	5/13
4 except Marine 4	0.35	0.55	0.40	49	20 or 13 + 5 <sup>h</sup>	8/13	19	10 /13	10, 2 ft	10/13
5 and Marine 4	0.32	0.55	NR	49	20 or 13 + 5 <sup>h</sup>	13/17	30 <sup>g</sup>	15/19	10, 2 ft	15/19
6	0.32	0.55	NR	49	20 + 5 or 13 + 10 <sup>h</sup>	15/20	30 <sup>g</sup>	15/19	10, 4 ft	15/19
7 and 8	0.32	0.55	NR	49	20 + 5 or 13 + 10 <sup>h</sup>	19/21	38 <sup>g</sup>	15/19	10, 4 ft	15/19

### HEAT LOSS CALCULATIONS

\***R,U-FACTOR\_CODE** COMPLIANCE CALCULATIONS WILL WANT TO KNOW R VALUE FOR THE WALLS AND U FACTOR FOR THE FENESTRATION. THE U VALUE FOR WINDOWS AND GLASS DOORS (FENESTRATION) IS REQUIRED BY MANUFACTURERS TO BE VERIFIED AND LISTED. THE ZONE 2 CODE REQUIRED .40 IS EQUIVALENT OF AN R-2.5, ZONES 3-4 REQUIRED .35 AN EQUIVALENT OF R-2.9, ZONES 5-8 REQUIRED .32 AN EQUIVALENT OF R-3.1. COMPARED TO THE WALLS VALUE OF SAY R-20. NOTE THE BETTER CARDINAL GLASS IS RATED AT .25 EQUIVALENT TO R-4. FENESTRATION IS A WEAK LINK FROM THE BASIC STANDPOINT OF HEAT GAIN/LOSS THRU THE WALLS. THESE COMPARATIVE VALUES FOR THE FENESTRATION'S U VALUES CAN BE MANIPULATED IN THE REScheck SOFTWARE TO YIELD A PERCENTAGE OF DIFFERENCE IN PERFORMANCE FOR THE TOTAL ENCLOSURE.

\***HEAT GAIN/LOSS\_ENERGY** CALCULATIONS WILL USE THE R WALL VALUES AND FENESTRATION U FACTOR TO DETERMINE BASIC HEAT LOSS AND GAIN. HEAT LOSS IS CALCULATING INTERIOR HEAT BEING RELEASED THRU THE ENVELOPE TO THE COLDER OUTSIDE. HEAT GAIN IS CALCULATING EXTERIOR HEAT'S PENETRATION THRU THE ENVELOPE TO THE COOLER INSIDE.

\***SOLAR HEAT GAIN\_IS** A SPECIFIC CALCULATION EXAMINING DIRECT SUNLIGHT HITTING GLASS. THE GLASS ITSELF HAS A RATING CALLED THE SOLAR HEAT GAIN COEFFICIENT (SHGC). A LOWER NUMBER MEANS THE GLASS IS KEEPING MORE HEAT FROM PENETRATING AND THE HIGHER NUMBER MEANS MORE HEAT IS PENETRATING. THE CODE IS REQUIRING MINIMUMS FOR GLASS RATINGS AND ALL WINDOW AND DOOR MANUFACTURERS ARE SIMPLY REQUIRED TO MEET THOSE STANDARDS. THIS IS GOOD. BOTH LOWER U AND SHGC RATINGS HAVE SAVED A LOT OF ENERGY IN THE SINGLE FAMILY HOME.

\***GLASS TECHNOLOGY\_GLASS** SKYSCRAPERS HAVE BEEN AROUND A GOOD WHILE IN SOME SERIOUS HOT CLIMATES. GLASS TECHNOLOGY HAS HAD TO BE ADDRESSED BIG TIME. THE RESIDENTIAL GLASS MARKET HAS BENEFITED FROM THAT TECHNOLOGY.

\***ENERGY CALCULATIONS**, BECAUSE SOLAR HEAT GAIN CAN EFFECT AIR CONDITIONING LOADS IT NEEDS TO BE ACCURATELY CALCULATED. LOGIC SAYS SMALL RANCH STYLE HOMES WITH CONVENTIONALLY SIZED WINDOWS AND ROOF OVERHANGS DON'T NEED TO DEAL WITH A LOT OF SOLAR GAIN, BUT CONTEMPORARY DESIGNS WITH LARGE/TALL WINDOW ASSEMBLIES HAVE TO BE VERY CONSCIOUS. NEXT PAGE WILL GIVE SOME OUTLINE TO THE SIMPLE FACTORS INVOLVED.

### GLASS OPTIONS

\***BETTER DATA\_BOTH** WINDOW MANUFACTURER'S AND GLASS MANUFACTURERS HAVE PRETTY EFFECTIVE PRESENTATIONS OF THESE 4 MOST PRESENTED PERFORMANCE CATEGORIES.

\***U-FACTOR**\_THE U-FACTOR IS THE 'INSULATING' RATING.

\***SHGC**\_HOW WELL THE GLASS BLOCKS THE SUN'S HEAT

\***TRANSMITTANCE**\_HOW MUCH NATURAL LIGHT PASSES THRU THE GLASS.

\***UV PROTECTION**\_ULTRAVIOLET RAYS CAN ALTER THE COLOR OF MATERIALS- AND ARE A CAUSAL SKIN CANCER INGREDIENT.





\***BEWARE GLASS VALUES AND WINDOW UNIT VALUES**\_VALUES ARE RECORDED AT CENTER OF GLASS FOR GLASS ONLY PERFORMANCE. WINDOWS REQUIRE UNIT TESTING IN THEIR FRAMES AND IS A BETTER REAL TIME PERFORMANCE NUMBER.

### (FROM THE ANDERSEN WINDOW CATALOGUE)

GLASS	ENERGY		LIGHT	
	U-Factor <small>How well a product prevents heat from escaping.</small>	Solar Heat Gain Coefficient <small>How well a product blocks heat caused by sunlight.</small>	Visible Light Transmittance <small>How much visible light comes through a product.</small>	UV Protection <small>How well a product blocks ultraviolet rays.</small>
<b>SmartSun</b> <small>Thermal control center-treated glass with visible light transmittance below 0.60 and 44 g/l.</small>	●●●○	●●●●	●●●○	●●●●
<b>SmartSun with HeatLock Coating</b> <small>Applied to the room-side surface, it reflects heat back into the home and improves U-factor.</small>	●●●●	●●●●	●●●○	●●●●
<b>Low-E4</b> <small>Outstanding overall performance for climates where both heating and cooling costs are a concern.</small>	●●●○	●●●○	●●●○	●●●○
<b>Low-E4 with HeatLock Coating</b> <small>Applied to the room-side surface, it reflects heat back into the home and improves U-factor.</small>	●●●●	●●●○	●●●○	●●●○
<b>Sun</b> <small>Outstanding thermal control in southern climates where less solar heat gain is desired.</small>	●●●○	●●●●	●●●○	●●●○
<b>PassiveSun</b> <small>Ideal for windows placed with maximum south-facing exposure where solar heat gain is desired.</small>	●●●○	●●●○	●●●○	●●●○
<b>Triple-Pane with Low-E Coatings on two surfaces</b> <small>Three panes of glass combine with visible light gas filled air or low-E coatings to provide advanced energy performance.</small>	●●●○	●●●○	●●●○	●●●○
<b>Clear Dual-Pane</b> <small>High visibility with basic thermal performance.</small>	○●○●	○●○●	●●●●	○●○●

Center-of-glass performance only. Ratings based on glass exposure as of March 2016. Visit us at [www.andersen.com](http://www.andersen.com) for more information on ENERGY STAR®-qualified products and performance data.

### (FROM THE GUARDIAN GLASS WEB SITE)

 <p><b>ClimaGuard 80/70</b> ENERGY STAR® Northern Zone Selectively lets visible light in to brighten and warm northern homes naturally, and provides insulation to stop heat from escaping</p>	 <p><b>ClimaGuard 72/57</b> ENERGY STAR® Northern and North-Central Zones Provides ample light, solar heat gain and retains heat indoors in climates with cold winters</p>	 <p><b>ClimaGuard 53/23</b> South-Central and Southern ENERGY STAR® Zones Cools homes in warm, southern climates with triple silver protection to lower solar heat gain and U-value</p>	 <p><b>ClimaGuard IS-20</b> All ENERGY STAR® Zones Enhances performance by lowering U-value of standard low-E windows to help meet energy codes</p>
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### SETTING THE SOLAR HEAT GAIN CRITERIA

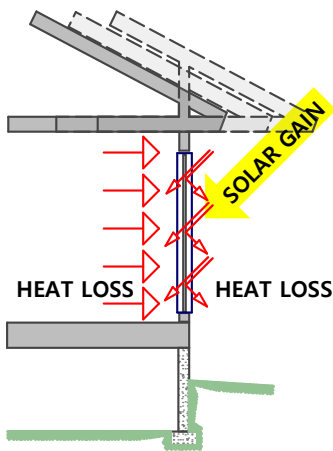
**\*POWER OF THE SUN**\_A SIMPLE WAY TO EXPERIENCE SOLAR RADIATION IS TO PICK A COOL CLEAR (MID)DAY AND STEP IN AND OUT OF THE SUN WEARING SHIRTSLEEVES. THE WARMTH THE SUN MAKES AVAILABLE CAN BE FELT INSTANTANEOUSLY. ONE CAN EXPERIENCE SOMETHING SIMILAR INSIDE BY STEPPING INTO AND OUT OF DIRECT SUNLIGHT AT A WINDOW. NOT AS INTENSE MAYBE BUT STILL A VERY REAL PRESENCE. SO THE QUESTION IS WHETHER THAT (HEAT GAIN) IS WELCOME OR NOT.

**\*PASSIVE SOLAR THINKING**\_THE WHOLE IDEA OF PASSIVE SOLAR DESIGN IS TO WELCOME THAT SOLAR GAIN, AND STORE IT IN A HEAT SINK FOR DISTRIBUTION BACK INTO THE SPACE AS INTERIOR TEMPERATURES COOL DOWN AFTER SUNSET.....USING SOLAR GAIN REQUIRING FAIRLY SPECIFIC MANAGEMENT TECHNIQUES.

**\*REDUCE SOLAR GAIN THINKING**\_SAYS THAT MANAGING THAT PASSIVE SOLAR ENERGY IS JUST TOO DIFFICULT- AND ULTIMATELY RESULTS IN INCONSISTENCIES AND INEFFICIENT ENERGY MANAGEMENT. SO THE SMART THING TO DO IS MINIMIZE SOLAR GAIN WITH PROPER GLASS SIZING, POSITION, APPROPRIATE ROOF OVERHANGS AND BLANKET THE HOUSE WITH AIR TIGHT HIGH PERFORMING INSULATION. GET IN ABSOLUTE CONTROL OF ENERGY CONSUMPTION.

**\*TRADITIONAL DESIGN**\_THE SUNROOM WAS ONCE A SPACE AND FUNCTION IN THE AMERICAN HOME. A CENTERHALL DESIGN WOULD HAVE THE SUNROOM ON ONE SIDE OF THE HOME USUALLY ACCESSIBLE FROM THE LIVING SPACE THROUGH GLASS DOORS. THIS ALLOWED THE SUN ROOM (OR CONSERVATORY) TO HAVE GENEROUS PERIMETER GLASS ON 3 WALLS, AND PROVIDE THAT WELL LIT AND OUTSIDE FEELING SPACE SO VALUABLE ON CERTAIN WEATHER DAYS. SUBJECT TO BEING SIMPLY TOO COLD IN WINTER AND OR POSSIBLY TOO HOT IN SUMMER. RETREAT FROM TOO COLD AND TOO HOT WAS AVAILABLE IN THE ADJACENT 'INTERIOR' LIVING SPACE.

**\*MANY INBETWEEN OPTIONS**\_TODAYS GLASS OPTIONS MAKE ALL THREE OPTIONS NOTED ABOVE MORE VIABLE. AND THEY MAKE OTHER INBETWEEN OPTIONS VIABLE AS WELL.



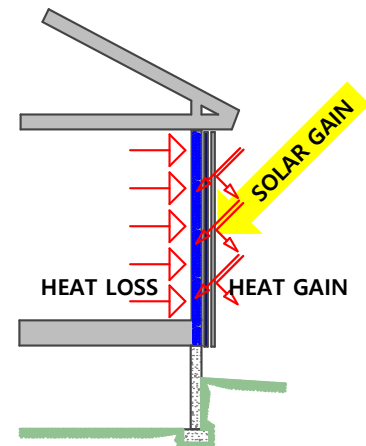
### MANAGING SOLAR HEAT GAIN

**\*LATITUDE**\_IS A FIXED CONDITION OF A SITE SELECTION, SO THE SUN'S EXACT ANGLE IS A PREDICABLE YEAR ROUND, AND THEREFORE A DESIGN CONDITION.

**\*ORIENTATION**\_BASED ON SITE CONDITIONS AND LIMITS ON THE BUILDING FOOTPRINT POSITIONING, THE ORIENTATION MAY BE UNDER THE DESIGNERS MANAGEMENT. CHAPTER d4 ATTEMPTS TO PRESENT AND SUMMARIZE THESE SITE BASED CONSIDERATIONS. THIS IS SUGGESTING THE CONTROL OF GLASS FACING EAST, SOUTH AND WEST.

**\*OVERHANG**\_THIS IS ALWAYS UNDER THE CONTROL OF THE DESIGN. AND CLEARLY WANTS TO BE CONSIDERED EARLY IN A DESIGN. FOR EXAMPLE LIVING SPACES ON THE LOWER OF 2 FLOORS DON'T HAVE ROOF TYPE PROTECTION UNLESS IT IS CONSCIOUSLY DESIGNED IN.

**\*SHGC**\_SEE GLASS OPTIONS. SELECTING A SHGC RATING FOR SPECIFIC THE POSITIONING OF GLASS IN A DESIGN IS BEING DONE MORE AND MORE. THE TYPICAL APPLICATION IN PASSIVE SOLAR THINKING IS USING A HIGHER SHGC RATED GLASS ON SOUTH WALLS, A LOWER RATED SHGC GLASS ON EAST AND WEST WALLS, AND A LOW U-FACTOR GLASS ON NORTH WALLS. SOME WINDOW MANUFACTURERS WILL ALLOW GLASS SPECIFICATION WITHIN A HOUSE ORDER USING THE SAME WINDOW TYPE.

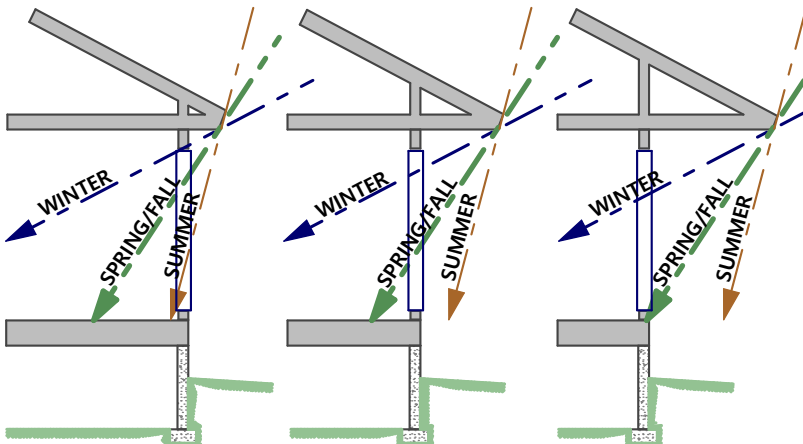


### SOLID WALL OPTIONS

**\*GENERAL**\_ALTHOUGH WE MEASURE THE SOLAR GAIN THRU GLASS, IT IS OBVIOUS THE OPAQUE WALLS ARE SUBJECT TO THE SAME ENERGY FROM THE SUN. HOW DOES THAT PLAY INTO ENERGY CONSUMPTION AND HOUSE HEALTH? THIS PROJECT HONESTLY DOES NOT KNOW. OPAQUE WALLS ARE NOT A DESIGN FACTORS IN THE SOFTWARE THIS PROJECT IS FAMILIAR WITH.

**\*WHAT WE KNOW**\_MATERIALS AND COLORS HAVE HEAT AND LIGHT REFLECTIVE COEFFICIENTS, AND HAVE HEAT RETENTION COEFFICIENTS. THE EASY EXAMPLE IS A DARK COLORED METAL SIDING HEATING UP QUICKLY, AND DISSIPATING HEAT QUICKLY. A LIGHT COLOR METAL WILL REFLECT/DEFLECT SOME PERCENTAGE OF THAT HEAT. A FULL 5" STONE VENEER WILL HEAT UP SLOWLY AND DISSIPATE THAT GAINED HEAT SLOWLY. THAT STONE IS PLAYING THE ROLE OF THERMAL MASS- AS WOULD MOST MASONRY MATERIALS.

**\*THE REST OF THE WALL ASSEMBLY**\_CONTAINS THE HYGROTHERMAL DEFENCE PACKAGE AND IS THERE TO MANAGE THAT SUN'S INTERPLAY WITH THE OUTSIDE PROTECTIVE SIDING MATERIAL. SO THE QUESTION OF THE ENERGY BASED IMPORTANCE OF THAT OUTER SKIN REMAINS UNCLEAR TO THIS PROJECT. IT IS NOT A CODE CONSIDERATION



THIS GRAPHIC IS SHOWING THE ROOF OVERHANG LENGTH ONLY AS ONE FIXED VARIABLE. THE SUN'S POSITION RELATIVE TO THE HOUSE IS ALWAYS IN FLUX.

### SOLAR GAIN CALCULATIONS

**\*HVAC CALCULATIONS**\_WILL NEED TO KNOW THE BELOW TO ASSESS SOLAR HEAT GAIN.

**\*LATITUDE**\_OF THE SITE WILL ESTABLISH THE SUNS ALTITUDE.

**\*ORIENTATION**\_EAST, SOUTH, WEST ORIENTATION OF WALLS/WINDOWS.

**\*OVERHANG DATA**\_ROOF OVERHANG DATA WILL DETERMINE EXTENT OF SUNS DIRECT CONTACT WITH THE GLASS.

**\*SHGC**\_WILL DETERMINE THE PERCENTAGE OF THAT SUN RADIATION THAT WILL PENETRATE TO THE INTERIOR.

**\*ORIENTATION CALCULATIONS**\_THIS PROJECT IS NOT EXPERIENCED ENOUGH WITH AVAILABLE HVAC/ENERGY SOFTWARES TO KNOW HOW THESE GEOMETRICALLY COMPLICATED PERMUTATIONS ARE INCORPORATED. REMEMBER THE SUN POSITION IN RELATION TO THE HOME CHANGES MINUTE BY MINUTE ALL YEAR LONG SO NECESSARILY DOES THE SOLAR GAIN. AND SUN'S INTENSITY IS OF COURSE NOT CONSISTENT.

## **COMPLIANCE (IRC 2018)**

\***CHAPTER 11** IS TITLED ENERGY EFFICIENCY AND IS PART OF THE 2018 IRC. (THIS CHAPTER REFERENCES IN EVERY SECTION THE SAME CONTENT AS FOUND IN THE 2018 IECC (INTERNATIONAL ENERGY CODE COUNCIL). THE IECC CODE USES A PREFIX 'R' WHICH IS UNFORTUNATELY CONFUSING BECAUSE ALL BUT THIS ENERGY CHAPTER IN THE BASE IRC ALSO USES THAT PREFIX 'R'. THE IECC ENERGY CODE IS IT OWN (BIG FAT) BOOK.

\***CHAPTER 11 COMPLIANCE INQUIRY** IT IS NECESSARY, PARTICULARLY WITH THE ENERGY COMPLIANCE THIS CHAPTER TALKS ABOUT, TO REQUEST LOCAL CODE COMPLIANCE REQUIREMENTS. THIS IS SUGGESTED BOTH TO KNOW WHAT WILL BE REQUIRED, AND TO AVOID BEING OVERWHELMED WITH REQUIREMENTS NOTED BELOW. REMEMBER EACH STATE AND LOCAL CODE JURISDICTION MAY OR MAY NOT HAVE ADOPTED THIS 2018 IRC CODE, AND MAY OR MAY NOT HAVE PRODUCED THEIR OWN CUSTOMIZED VERSION. SO REQUIREMENTS WILL VARY. AS A 'FOR INSTANCE' NORTH CAROLINA DELETED N1101.5 AND N1101.5.1 IN ITS VERSION OF THE 2018 IRC.

\***ARCHITECTURAL/DESIGN DOCUMENTS** TRADITIONALLY AND TYPICALLY DO NOT INCLUDE ALL THE ENERGY SPECIFIC CONTENTS NOTED BELOW (N1101.5). THERE ARE EXCEPTIONS TO THIS. SOME MORE COMPLETE ARCHITECTURAL SERVICES MAY ELECT TO INCORPORATE ALL ENERGY/MECHANICAL REQUIREMENTS AND APPROPRIATE DRAWINGS INTO ONE COMPREHENSIVE PACKAGE. THESE 2 CODE SECTIONS ARE INCLUDED FOR REFERENCE.

### **N1101.5 (R103.2) Information on construction documents.**

Construction documents shall be drawn to scale on suitable material. Electronic media documents are permitted to be submitted when approved by the building official. Construction documents shall be of sufficient clarity to indicate the location, nature and extent of the work proposed, and show in sufficient detail pertinent data and features of the building, systems and equipment as herein governed. Details shall include the following as applicable:

1. Insulation materials and their R-values.
2. Fenestration U-factors and solar heat gain coefficients (SHGC).
3. Area-weighted U-factor and solar heat gain coefficient (SHGC) calculations.
4. Mechanical system design criteria.
5. Mechanical and service water heating systems and equipment types, sizes and efficiencies.
6. Equipment and system controls.
7. Duct sealing, duct and pipe insulation and location.
8. Air sealing details.

### **N1101.5.1 (R103.2.1) Building thermal envelope depiction.**

The building thermal envelope shall be represented on the construction documents.

## **STANDARD COMPLIANCE METHODS**

**R VALUE (N1102.1.3)** \_COMPONENT COMPLIANCE (c9.4).

**U VALUE (N1102.1.4)** \_ ASSEMBLY COMPLIANCE (c9.4)

**UA ALTERNATIVE (N1102.1.5)** \_TOTAL THERMAL ENVELOPE COMPLIANCE (c9.5, c9.6)

## **PERFORMANCE OPTIONS TO ACHIEVING CODE COMPLIANCE**

**ONE REASON SIMULATED PERFORMANCE AND ERI COMPLIANCES EXIST IS TO OPEN THE DOOR TO NON TRADITIONAL CONSTRUCTIONS WHILE MEETING ENERGY STANDARDS.**

### **SECTION N1105 SIMULATED PERFORMANCE ALTERNATIVE**

\*PERFORMANCE BASED COMPLIANCE-STARTS WITH AN ENERGY ANALYSIS OF THE PROJECT BASED ON ALL CODE PRESCRIBED MINIMUMS. THE (ANNUAL) ENERGY REQUIRED BY THAT DESIGN IS THE BASELINE. THE PROJECT CAN THEN DEVIATE FROM PRESCRIBED REQUIREMENTS BUT MUST MEET OR REDUCE THOSE (ANNUAL) ENERGY REQUIREMENTS.

\*ANY CODE MINIMUMS DESIGNATED 'MANDATORY' MUST BE MET.

\*PRE-APPROVED ENERGY ANALYSIS SOFTWARE/DOCUMENTATION IS REQUIRED. 3RD PARTY INVOLVEMENT REQUIRED.

### **SECTION N1106 ENERGY RATING INDEX (ERI) COMPLIANCE ALTERNATIVE aka HERS rating**

\*SIMILAR TO THE ABOVE IN BEING AN ENERGY BASED ANALYSIS, BUT RESTRICTED TO A SPECIFIC VERIFICATION (A GRADE CARD) TECHNIQUE QUALIFIED BY A 'STANDARD' TITLED 'RESNET/ICC 301'. A PROPOSED PROJECT IS EVALUATED ON PAPER BASED ON A ZERO TO 100 NUMERICAL SYSTEM. THE ENTIRE HOUSE IS ENERGY ANALYZED AND AWARDED POINTS WHEREIN LOWER IS BETTER. ZERO IS ZERO ENERGY.

\*PRE-APPROVED ENERGY ANALYSIS SOFTWARE/DOCUMENTATION IS REQUIRED. 3RD PARTY INVOLVEMENT REQUIRED.

\*THE MORE WELL KNOWN 3RD PARTY SERVICE IS AVAILABLE FROM A CERTIFIED **HERS** RATER (HOME ENERGY RATING SYSTEM).

## **THE SPEED OF CHANGE IN HYGRO-THERMAL AND SUSTAINABLE DESIGN CONSIDERATIONS**

\***THIS CHAPTER** AND OTHER PAGES AND CONTENT THIS PROJECT DEALING WITH ABOVE NOTED TOPICS RUN THE RISK OF GETTING OUT DATED. BOTH KNOWLEDGE ABOUT, AND CODE COMPLIANCES FOR THESE TOPICS ARE CHANGING MORE QUICKLY THAN MOST OF THE GENERAL CONSTRUCTION TOPICS. AS/WITH CLIMATE CHANGE SCIENCE AND CONSEQUENT NECESSARY REGULATION, WE ARE LIKELY HEADED TOWARD AN EVEN MORE ACCELERATED PACE OF CHANGE.

\***ENERGY CONSULTANCIES** PART OF THIS CHANGE HAS BEEN THE EVOLUTION OF A VERY LARGE COTTAGE INDUSTRY PROVIDING A WHOLE RANGE OF INFORMATIONAL, TESTING, AND COMPLIANCE SERVICES TARGETING ENERGY CONSERVATION AND SUSTAINABLE DESIGN. IMPORTANT, USEFUL, AND GENERALLY WELL INTENTIONED.

## **APPROACHES TO 3RD PARTY INVOLVEMENT**

\***CHOICES** GREEN BUILDING ADVOCACY ORGANIZATIONS, INDEPENDENT ENERGY AND SUSTAINABLE CONSULTANCIES, ARE MANY AND ALL OVER. THEY NEED TO BE LOCALLY RESEARCHED. ARCHITECTS, HVAC VENDORS, AND PV SOLAR PROVIDERS ARE ADDITIONAL VIABLE RESOURCES.

\***CERTIFICATIONS AND RATERS** GREEN BUILDING 'CERTIFICATION' PROGRAMS, AND ENERGY RATING COMPANIES ARE HERE TO STAY. THE GOVERNMENTS SPONSORED 'ENERGY STAR' PROGRAM, AND THE RESNET (NON-PROFIT) SPONSORED 'HERS' RATING SERVICE IS NATIONALLY AVAILABLE, AND CONSIDERED (AT LEAST BY NON-COMPETITORS) TO BE REASONED AND WELL DESIGNED. RESNET IS BEHIND THE REScheck SOFTWARE COMPLIANCE PACKAGE NOTED THIS CHAPTER.

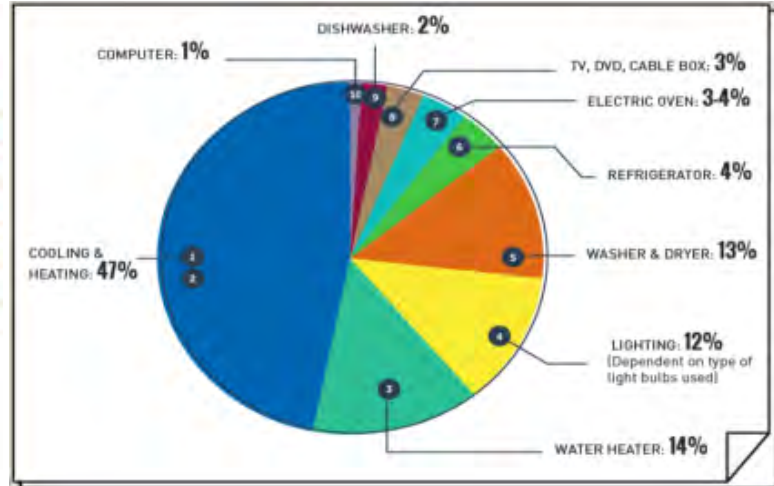
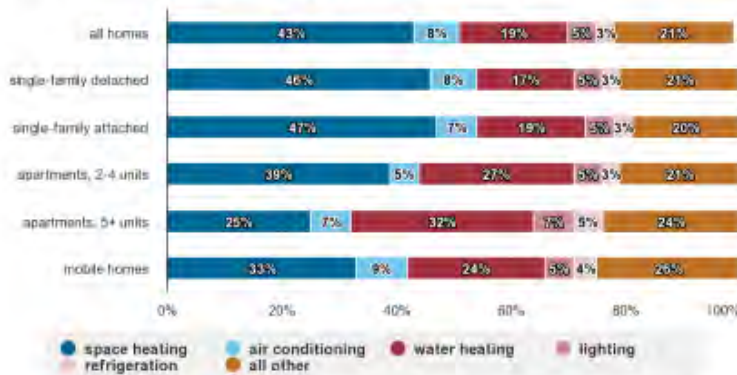


### MAKING THE COMPLEX SIMPLE(R)

\***THE COMPLEX**\_ONE BIG CHALLENGE PUTTING THIS DESIGN AND CONSTRUCTION GUIDE PACKAGE TOGETHER HAS BEEN DECIDING WHAT TO INCLUDE, AND HOW DEEP TO DIG. SCIENCE WOULD LET US DIG FOREVER. IT IS NOT THAT HARD TO GET LOST IN THE WEEDS, AND LOSE SITE OF THE ULTIMATE GOALS.

\***THE SIMPLE**\_THESE INSTRUCTIVE CHARTS BELOW (GOVERNMENT STATISTICS) GIVE US A HAND REVISITING THE IMMEDIATE GOAL. THE PIE CHART IS PARTICULARLY CLEAR INDICATOR OF THE PECKING ORDER OF ATTENTION AND CONCENTRATION. THE THERMAL ENVELOPE/HVAC SYSTEM IS CLEARLY THE BIG PLAYER AND BY FAR THE MORE COMPLICATED ONE. THE BALANCE OF THESE CATEGORIES OF ENERGY EXPENDITURE CAN BE RESEARCHED WITH OPTIONS AND BETTER SOLUTIONS BEING PRETTY EASY TO TRACK DOWN.

End-use consumption shares by types of U.S. homes, 2015



### FIND A GUIDING APPROACH

\***LIST BELOW**\_APPROACHES BELOW ARE ESSENTIALLY MAINSTREAM, AND COMPATIBLE WITH 'CONVENTIONAL' RESIDENTIAL CONSTRUCTION. THEY ALL ARE DIRECTLY RELATED TO ENERGY EFFICIENCY.

\***ABSOLUTE OR SYNTHESIZED APPROACH**\_ONE COULD PICK ANY OF THE BELOW AND GO FOR IT- MEANING LETTING THAT APPROACH BE THE DECISION MAKER. OR ONE CAN MIX AND MATCH A BIT TO SUIT THOSE NEEDS THAT ABSOLUTE SYSTEMS NOTORIOUSLY HAMSTRUNG. ITS ALL VALID, IT JUST HAS TO DO THE JOB.

\***BOTTOM LINE**\_WHATEVER APPROACH ONE MIGHT BE INCLINED TO PURSUE, AND TO WHATEVER LEVEL OF DEDICATION, THE VALUE OF HOOKING UP WITH A MEANS OF COMPUTERIZED ENERGY ANALYSIS IS HIGHLY RECOMMENDED. AS QUICKLY DEMONSTRATED, EVEN WITH THE NOT SO SOPHISTICATED (AND FREE) REScheck, ONE CAN MONITOR THE RAMIFICATIONS OF DESIGN CHANGES ALL ALONG THE DESIGN PATH TO ASSIST IN THOSE GOOD/BETTER/BEST DECISIONS. MORE SPOHIFICATED SOFTWARE OFFERING MORE FEEDBACK ON DECISIONS IS BETTER YET. VENDORS AND 3RD PARTY ENERGY FOLKS MAY NEED TO ASSIST.

### 1.CONTAIN THE THERMAL ENVELOPE

\***GUIDES**\_THE WHOLE IDEA OF DEFINING AND CONTAINING THE THERMAL ENVELOPE HAS BEEN FRONT AND CENTER THESE GUIDES. MAYBE THE BEST QUANTITATIVE INDICATOR IS THAT SQUARE FOOTAGE OF THERMAL ENVELOPE.

\***SIMPLE AND SMALL**\_COMMON SENSE TELLS US SIMPLE AND SMALL IS ONE SUSTAINABLE APPROACH. IT IS ALSO NOT SUITABLE TO EVERYONE.

\***NOT SO SIMPLE, NOT SO SMALL**\_DESIGNS MANAGE SIZE AND SHAPE (d5) AND THERE ARE MORE AND LESS EFFICIENT WAYS TO INCREASE FOOTAGE. COMPLEXITY IN GEOMETRY WILL INCREASE THERMAL ENVELOPE FOOTAGE SO MAKE IT COUNT.

### 2.MAXIMIZE THE EFFICIENCY OF THE HVAC SYSTEM

\***ANY SYSTEM**\_ANY TYPE OF HEATING AND OR COOLING 'SYSTEM' WOULD CLEARLY WANT TO BE PERFORMING AT ITS HIGHEST EFFICIENCY.

\***DUCTED SYSTEMS**\_NUMBER ONE IS THE CORRECT SYSTEM SIZING. NUMBER TWO IS HAVING THE ENTIRE SYSTEM LOCATED INSIDE CONDITIONED SPACE. NUMBER THREE IS HIGHER EFFICIENCY EQUIPMENT. AND THEN DESIGNING GEOMETRICALLY STRAIGHTFORWARD DUCT RUNS AS IS POSSIBLE, WITH A RETURN SYSTEM LETTING THAT SUPPLY SIDE DO ITS BEST JOB.

### 3.PASSIVE SOLAR

\***THE STRICT PASSIVE SOLAR FORMULA**\_THERE ARE RULES AND REGULATIONS ONE CAN SUBSCRIBE TO FOR A HOME TO ACHIEVE PASSIVE SOLAR STATUS. THIS CAN BE AN ISSUE IF ONE IS PURSUING TAX CREDITS. WHETHER ONE IS AFTER TAX CREDITS OR NOT THOUGH, THOSE RULES OF DESIGN ARE IMPORTANT TO KNOW. THEY SET THE STAGE FOR MAXIMUM EFFICIENCY/EFFECTIVENESS, SO AS DESIGN GUIDELINES ARE VALUABLE. ONE CAN CHOOSE TO FOLLOW THOSE 'RULES' TO THE LETTER, OR TO INTERPRET/UTILIZE CREATIVELY.

\***THE UNIVERSAL PASSIVE SOLAR WARNING**\_THE PRIME IDEA IS TO CAPTURE (FREE) HEAT. OVERHEATING IN FACT IS A COMMON REAL PROBLEM. WHICH IS UNCOMFORTABLE AND COUNTER PRODUCTIVE.

### 4.THE PASSIVE HOUSE APPROACH

\***HISTORY**\_EASY TO SEARCH THE HISTORY AND PURPOSE OF THE PASSIVE HOUSE- WHICH IS INTERESTING AND ENLIGHTENING. AND IT WILL PUT THE WHOLE CERTIFICATION SIDE OF THE PASSIVE HOUSE INITIATIVE IN PERSPECTIVE. ALTHOUGH A CERTIFICATION BASED INITIATIVE THERE IS PLENTY OF EFFICIENCY CONTENT TO LEARN ABOUT.

\***IN THE US**\_www.PHIUS.org (Passive House Institute,US) www.PHAUS.org (Passive House Alliance,US)

\***GENERAL**\_ENERGY PERFORMANCE IS THE GOAL. INSULATING AND SEALING EXTREMELY WELL IS PART OF THE DEAL.

\***ENERGY RECOVERY VENTILATION(ERV/HEAT RECOVERY VENTILATION(HRV)**\_THESE ARE VENTILATION AIR 'EXCHANGERS' THAT CAN BECOME PART OF ANY SYSTEM, BUT ARE A CENTRAL AND SIGNIFICANT PLAYER IN THE PASSIVE HOUSE APPROACH. A LITTLE COMPLICATED AND NEEDS PROPER RESEARCH. THEIR ROLE REDUCES THE ENERGY REQUIREMENTS FOR MAINTAINING COMFORT.

### 5.ACTIVE SOLAR

\***THE GREAT BAND-AID**\_PHOTOVOLTAIC SOLAR PANELS OR ROOFING IS OFTEN A GREAT OPTION IN DECREASING USE OF DIRTY ENERGY. IT CAN BE EMPLOYED AT ANY SCALE. AND IT PERFORMS INDEPENDENTLY FROM THE HOUSE, AND IN FACT FROM EVERY APPROACH NOTED ABOVE. FOR THOSE WHO CARRY SOME SENSE OF RESPONSIBILITY ABOUT ENERGY USE AND CONSEQUENT CLIMATE CHANGE, AND DON'T WANT TO BE HAMSTRUNG BY BUILDING SHELL ENERGY EFFICIENCY RESTRICTIONS, IT OFFERS A PRETTY GOOD OUT. NEEDS A LOT OF SOUTH FACING AREA-